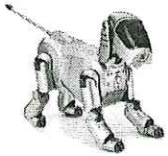




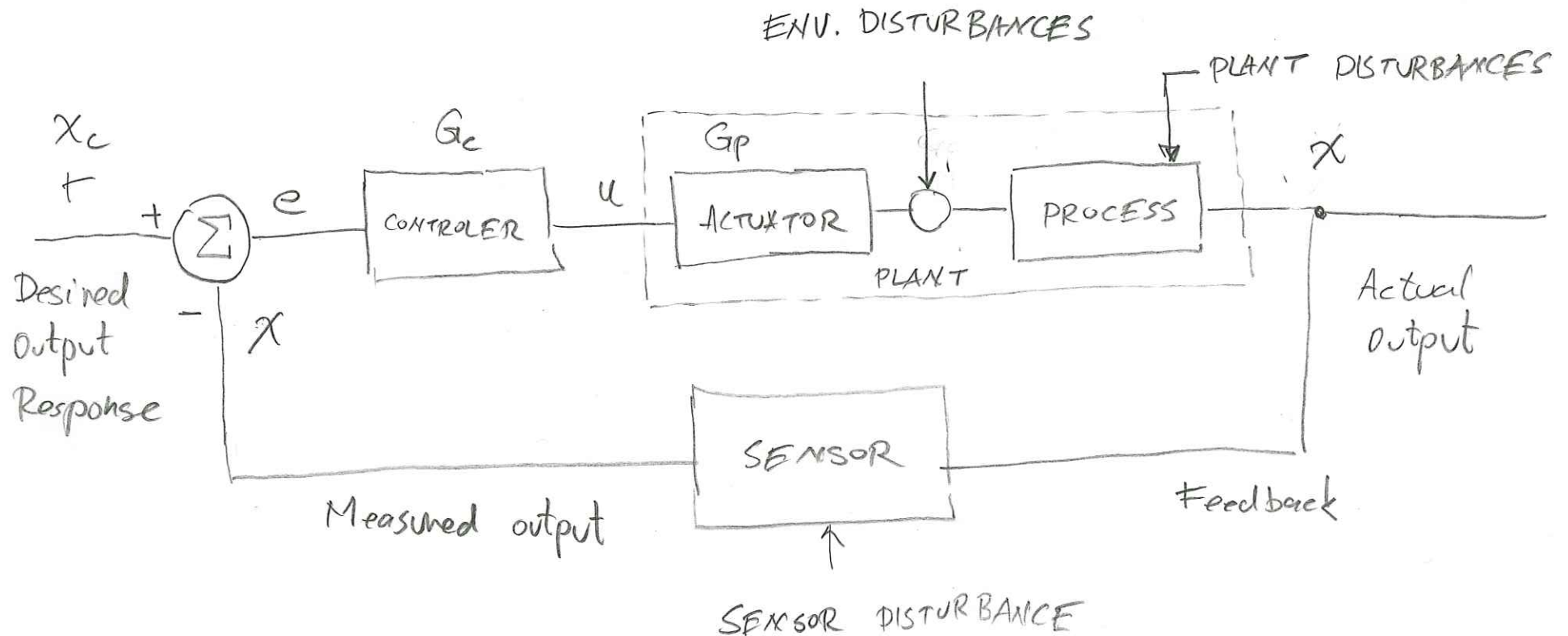
Control - PID

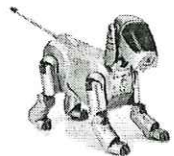


CONTROL - PID



CLOSE LOOP FEEDBACK CONTROL





PID - CONTROLLER - DEFINITION

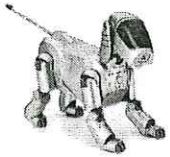
P - Proportional $\rightarrow k_p$

PID $\rightarrow$ I - Integral $\rightarrow k_i$

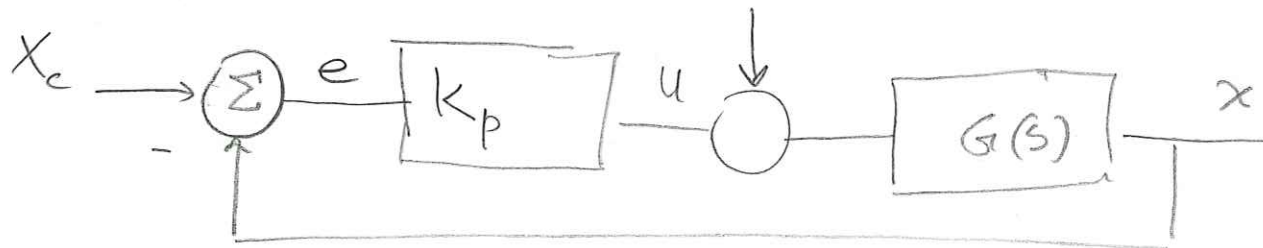
D - Derivative $\rightarrow k_d$

$$u(t) = k_p e(t) + k_i \int e(\tau) d\tau + k_d \frac{d}{dt} e(t)$$

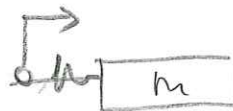
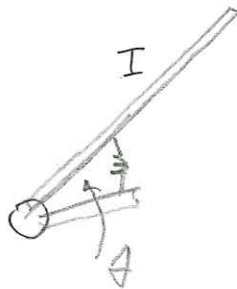
$$U(s) = E(s) \left[k_p + k_i \frac{1}{s} + k_d s \right] = E(s) = \frac{k_p s + k_i + k_d s^2}{s}$$



PID - CONTROLLER - (P) - PROPORTIONAL CONTROL



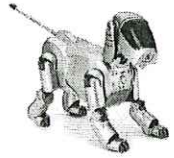
$$u = -k_p (x - x_c) = -k_p e$$



↑ SPRING

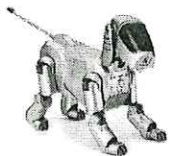
$$F = -k \Delta x$$





(P) - Problems

- ① ENERGY - k_p (spring) Does not remove energy out of the system
- ② RESONANCE - If the input x_c will match the natural frequency of the system $\rightarrow$ Resonance
- ③ LARGE ACTUATORS - To have a very small error we need large springs i.e. large actuators



④ FORCE/ERROR - Force is generated only if a certain amount of error is generated

When $\text{error} \rightarrow 0 \Rightarrow F \rightarrow 0$

What if the error $e \rightarrow 0$ (No force)

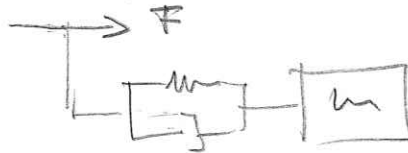
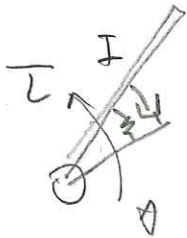
But we can measure velocity

⚠ $\Rightarrow$ We can predict the fact that we are about to build up an error



PID - CONTROLLER - (D) - DERIVATIVE CONTROLLER

$$u = -k_d (\dot{x} - \dot{x}_c) = -k_d \dot{e}$$



↑ Damper

$$F = -bv = -b\dot{x}$$



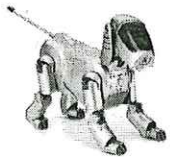
Advantage - Absorb energy $\rightarrow$ Remove energy out of the system



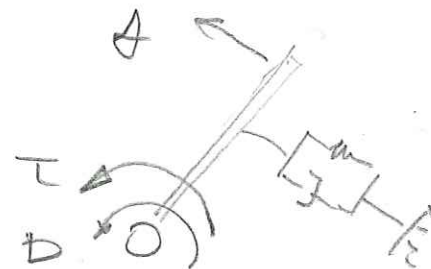
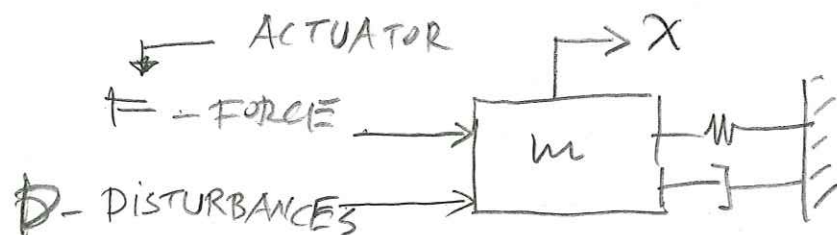
Summary

$k_p \rightarrow$ Spring ($F = kx$) - No force is applied until the system moves

$k_d \rightarrow$ Damper ($F = b\dot{x}$) - Anticipate motion



PD CONTROL - EXAMPLE

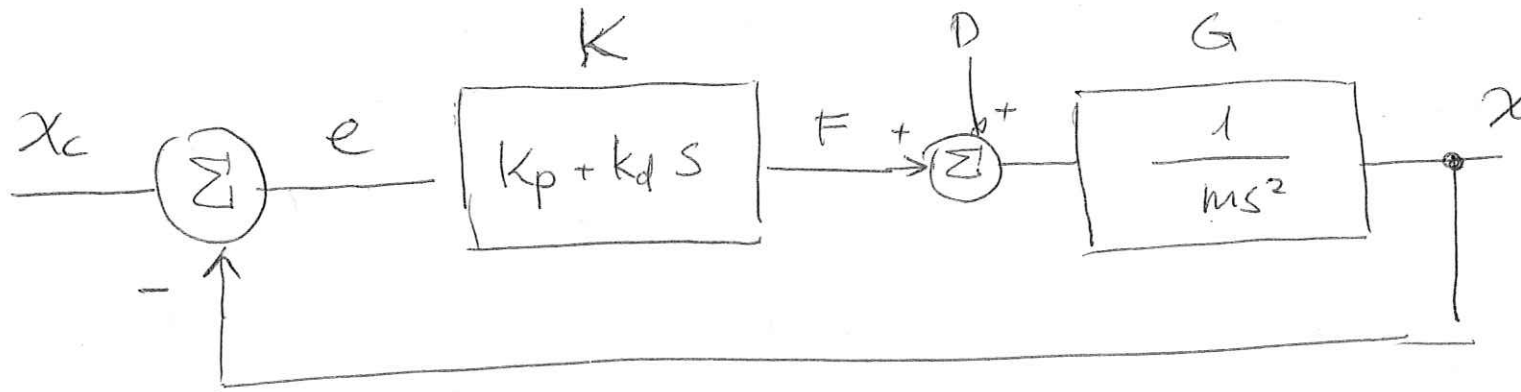


$$\uparrow \rightarrow \sum F = m\ddot{x}$$

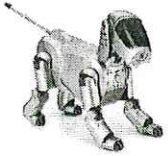
$$F + D = m\ddot{x}$$

$$F(s) + D(s) = m \ddot{x} s^2$$

$$\frac{X}{F(s) + D(s)} = \frac{1}{m s^2}$$



$$\begin{aligned} \frac{\text{Output}}{\text{Input}} &= \frac{\bar{X}}{\bar{X}_c} = \frac{K G}{1 + K G} = \frac{(k_p + k_d s) \frac{1}{m s^2}}{1 + (k_p + k_d s) \frac{1}{m s^2}} = \\ &= \frac{k_p + k_d s}{m s^2 + k_d s + k_p} = \frac{\frac{k_d}{m} s + \frac{k_p}{m}}{s^2 + \frac{k_d}{m} s + \frac{k_p}{m}} \end{aligned}$$



$$\omega_n = \frac{k_p}{m}$$

$$\zeta = \frac{k_d}{2m\omega_n} = \frac{k_d}{2} \sqrt{\frac{1}{m k_p}}$$

$$\frac{\bar{X}}{\bar{X}_c} = \frac{\frac{k_d}{m} s + \frac{k_p}{m}}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

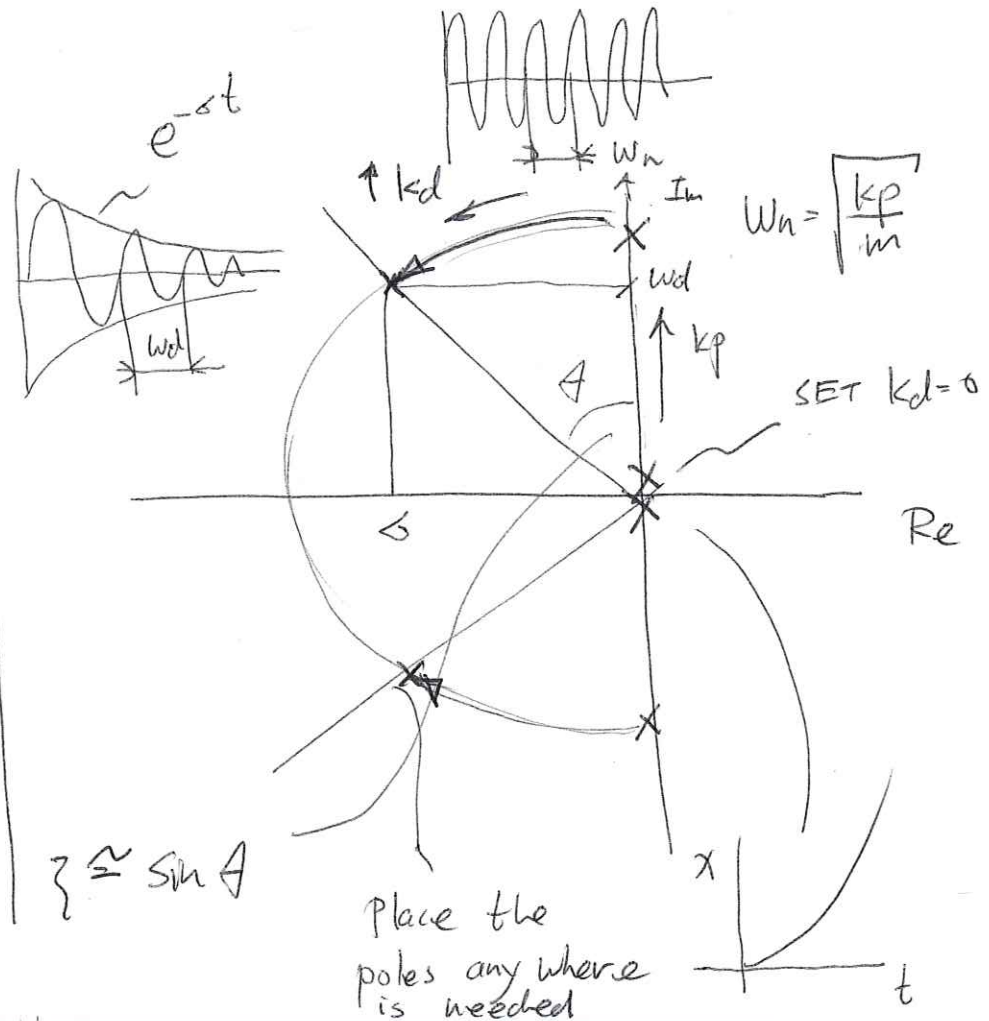


STEP 1 - { set $k_d = 0$

- [Increasing k_p
- [Move the poles along the Imaginary axis to the value of $\omega_n = \sqrt{\frac{k_p}{m}}$

STEP 2 - { set $k_p = \text{const}$

- [Increase k_d
- [The natural frequency stays the same but the damping increases





PD - ROOT LOCUS

$$KGH = \frac{k_d s + k_p}{m s^2} = k_d \left(s + \frac{k_p}{k_d} \right) / m s^2$$

POLES: $m s^2 = 0$

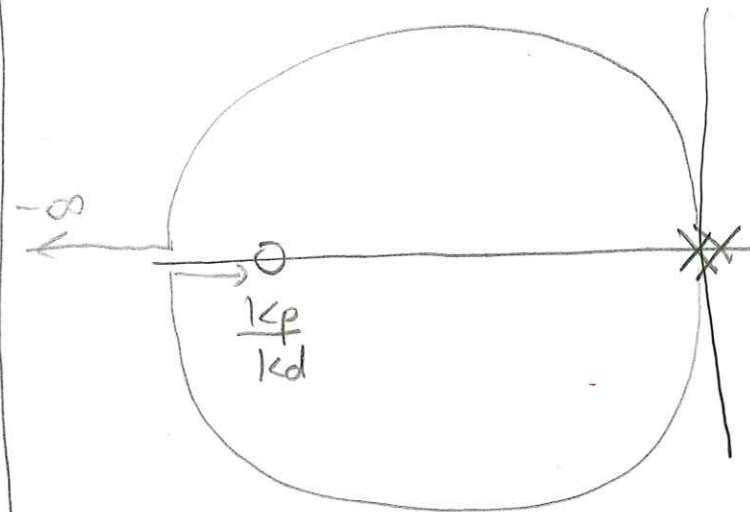
$$\Rightarrow p_1, p_2 = 0$$

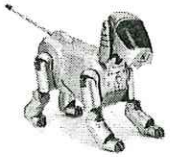
ZEROS: $s + \frac{k_p}{k_d} = 0$

$$z_1 = -\frac{k_p}{k_d}$$

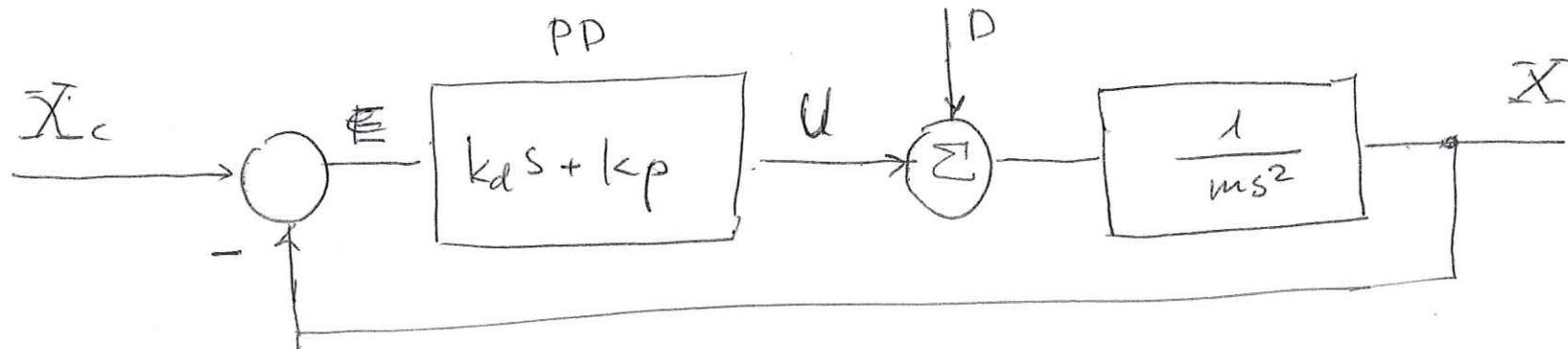
$$k_d \left[\frac{s + \frac{k_p}{k_d}}{m s^2} \right]$$

ROOT LOCUS





PID CONTROLLER - (I) - Integral



SUPER POSITION output $\rightarrow X = \underbrace{\left(\frac{X}{X_c} \right) \bigg|_{D=0}}_{\text{Transfer Function}} X_c + \underbrace{\left(\frac{X}{D} \right) \bigg|_{X_c=0}}_{\text{Transfer Function}} D$

Transfer Function

Input X_c

output X

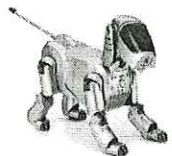
$D = 0$

Transfer Function

Input D

output X

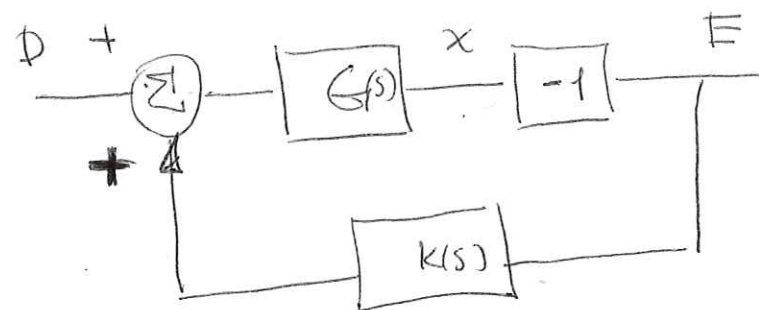
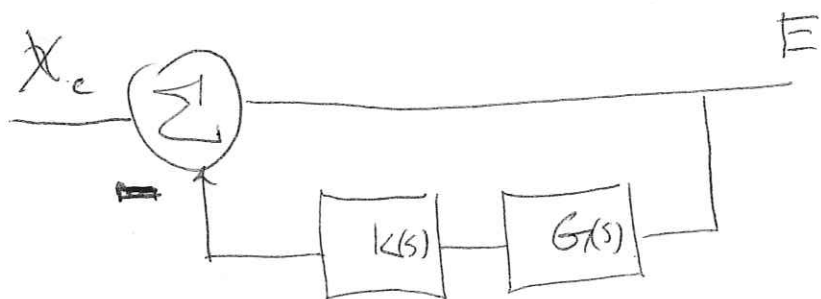
$X_c = 0$

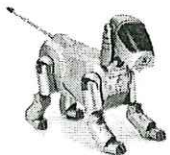


$$E = \left(\frac{E}{X_c} \right) \bigg|_{D=0} X_c + \left(\frac{E}{D} \right) \bigg|_{X_c=0} D$$

Input X_c ; Output E ↙

Input D ; Output E ↘





$$\left. \frac{E}{X_c} \right|_{b=0} = \frac{1}{1 + KG} = \frac{1}{1 + (k_d s + k_p) \cdot \frac{1}{ms^2}} = \frac{ms^2}{ms^2 + k_d s + k_p}$$

$$\left. \frac{E}{D} \right|_{X_c=0} = \frac{G}{1 \ominus KG} = \frac{-G}{1 - -GK_s} = -\frac{G}{1 + KG} = \frac{-\frac{1}{ms^2}}{1 + (k_d s + k_p) \frac{1}{ms^2}}$$
$$= -\frac{1}{ms^2 + k_d s + k_p}$$

Note the +
in the first
sum



Input

X_c 

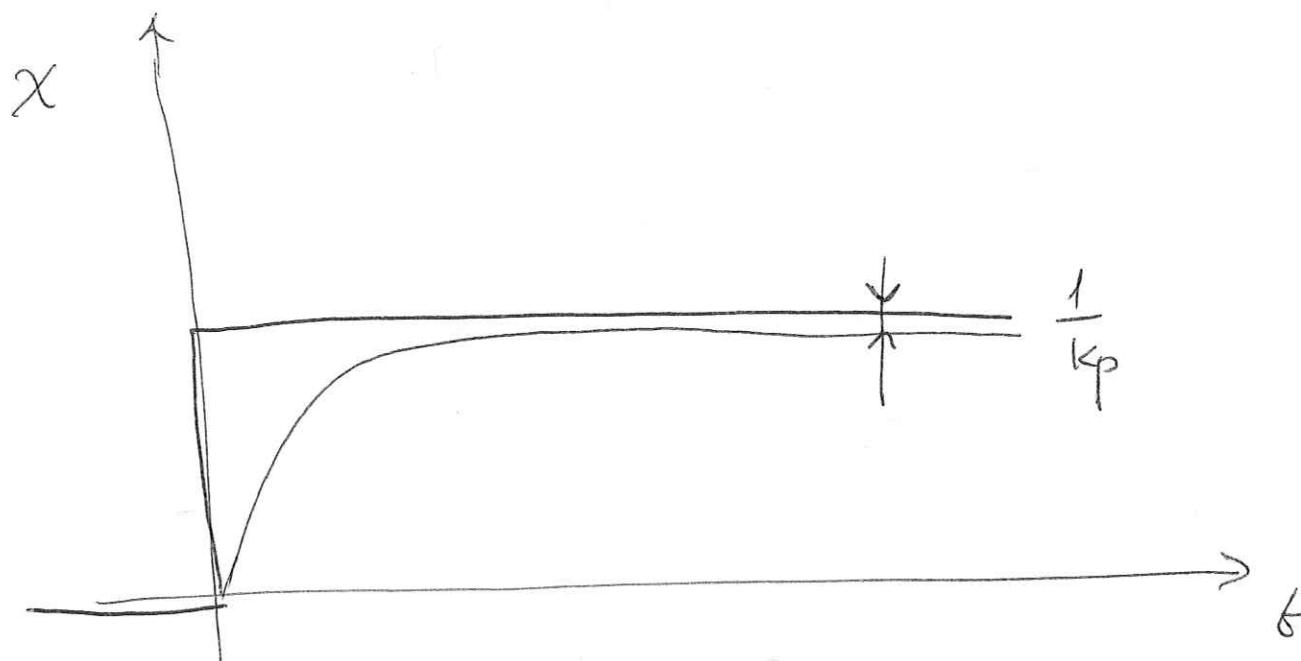
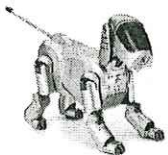
$$e_{ss} \Big|_{\frac{E}{X_c}} = \lim_{s \rightarrow 0} s \left[\frac{E}{X_c} \right] \left(\frac{1}{s} \right) = \lim_{s \rightarrow 0} \frac{ms^2}{ms^2 + kds + kp} = 0$$

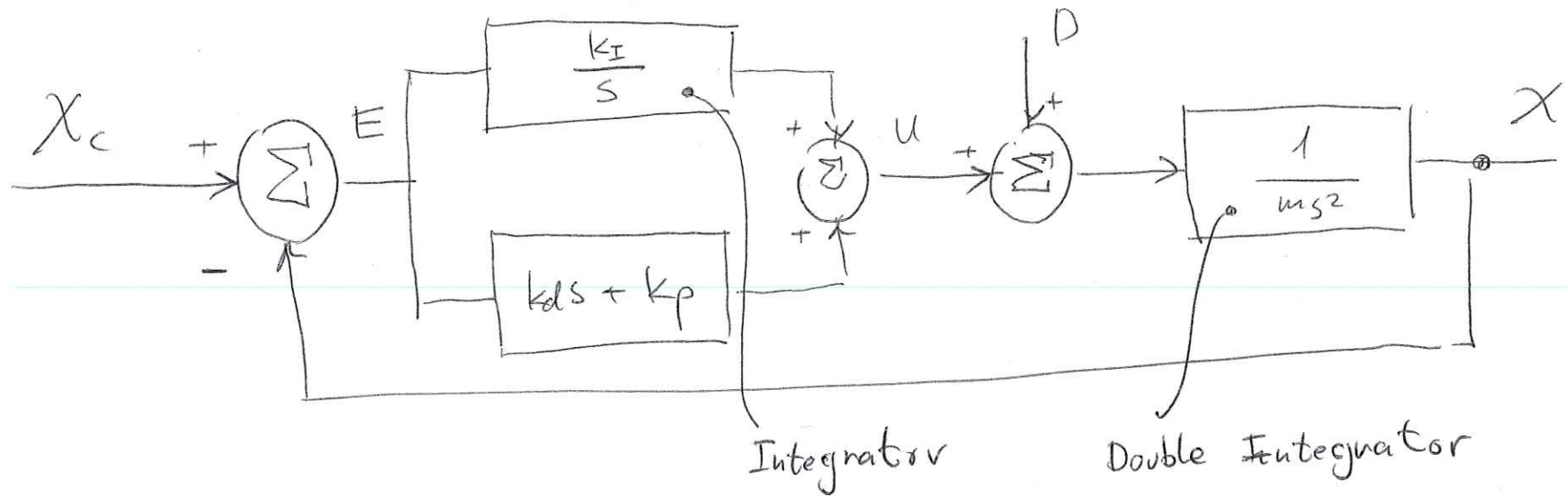
D 

$$e_{ss} \Big|_{\frac{E}{D}} = \lim_{s \rightarrow 0} s \left[\frac{E}{D} \right] \left(\frac{1}{s} \right) = \lim_{s \rightarrow 0} \frac{1}{ms^2 + kds + kp} = \frac{1}{kp}$$

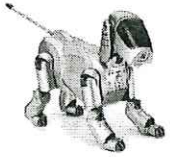
⊛ The disturbance generates a steady state error

$$\rightarrow \frac{1}{K_p}$$

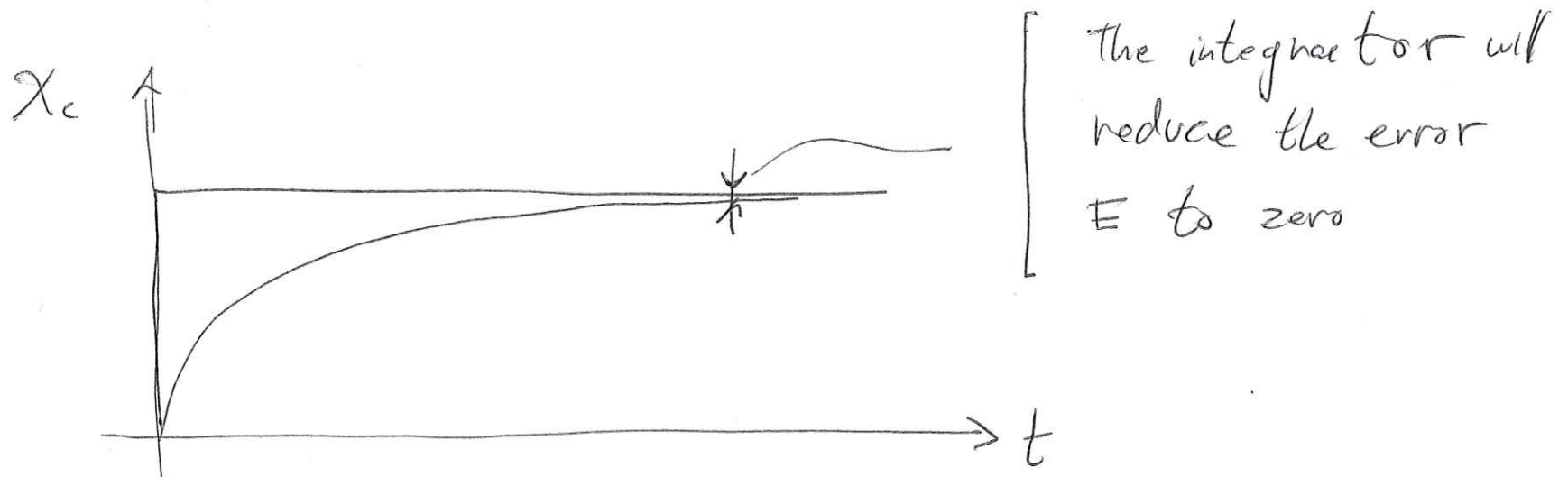


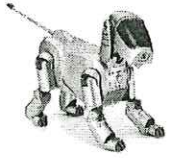


- * In Steady-state anything that goes into the integrator must be zero $\int(\text{error}) = 0$
- * If something gets into the Integrator it will start to accumulate and then we are not in steady state

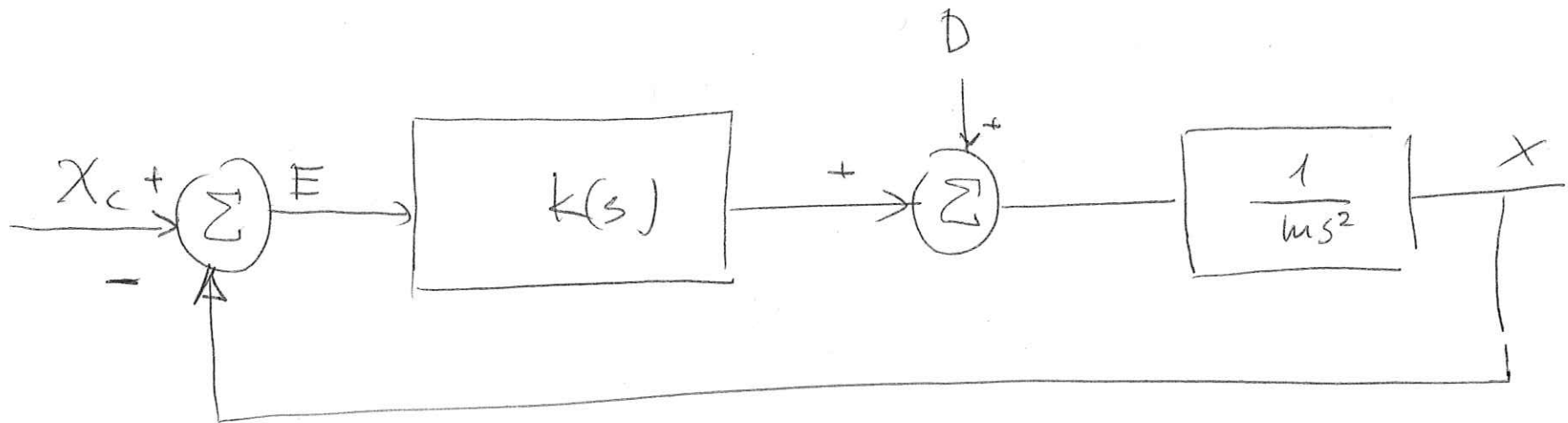
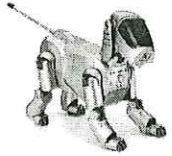


+ As a result $\rightarrow \begin{cases} U + D = 0 \\ E = 0 \end{cases}$

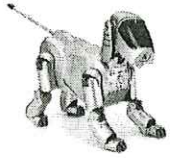




-
- * In general the value of the integral gain K_I should be small $\sim \frac{1}{100}$ of k_d or k_p
 - * The integral is a pole. Adding a pole to the system can make it unstable



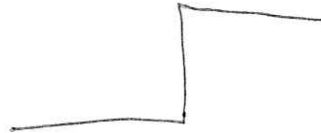
$$\text{PID} \rightarrow K(s) = \frac{k_I}{s} + k_d s + k_p = \frac{k_d s^2 + k_p s + k_I}{s}$$



$$\begin{aligned}\frac{E}{\Phi} &= - \frac{G}{1 + Gf} = - \frac{\frac{1}{ms^2}}{1 + \left(\frac{1}{ms^2}\right) \left(\frac{k_d s^2 + k_p s + k_I}{s}\right)} = - \frac{1}{ms^2 + \frac{k_d s^2 + k_p s + k_I}{s}} \\ &= - \frac{s}{ms^3 + k_d s^2 + k_p s + k_I}\end{aligned}$$



Input $\frac{1}{s}$

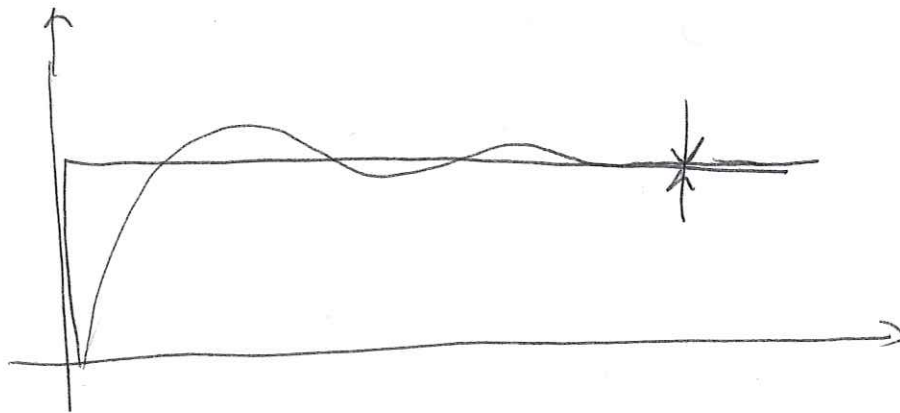


$$e_{ss} = \lim_{s \rightarrow 0} s \left[\frac{s}{ms^3 + kds^2 + kp s + k_I} \right] \frac{1}{s} = 0$$

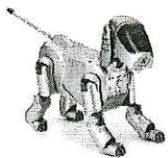
Input



$$\frac{1}{s} = 0$$



Tracking a step input
with a zero steady
state error



PID - ROOT LOCUS

$$\begin{aligned} KGH &= \frac{k_p + k_d s + k_I \frac{1}{s}}{m s^2} \\ &= \frac{k_p s + k_d s^2 + k_I}{m s^3} \\ &= k_d \left[\frac{s^2 + \frac{k_p}{k_d} s + \frac{k_I}{k_d}}{m s^3} \right] \end{aligned}$$

POLES

$$m s^3 = 0$$

$$P_1, P_2, P_3 = 0$$

ZEROS

$$s^2 + \frac{k_p}{k_d} s + \frac{k_I}{k_d} = 0$$

$$Z_1, Z_2 = \frac{-\frac{k_p}{k_d} \pm \sqrt{\left(\frac{k_p}{k_d}\right)^2 - 4 \frac{k_I}{k_d}}}{2}$$

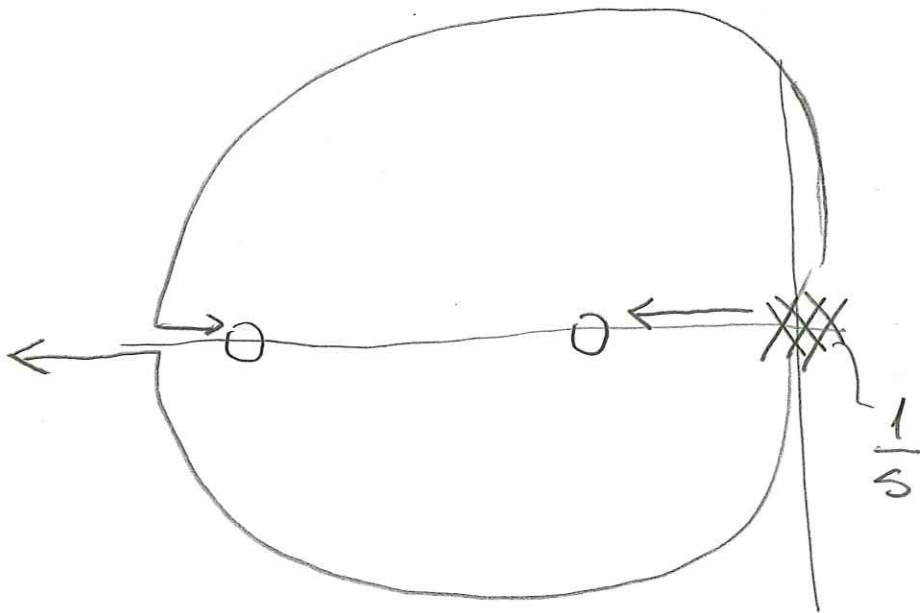
$$\Delta = \left(\frac{k_p}{k_d}\right)^2 - 4 \frac{k_I}{k_d}$$

$$\Delta > 0 \rightarrow 2 \text{ Real Zero}$$

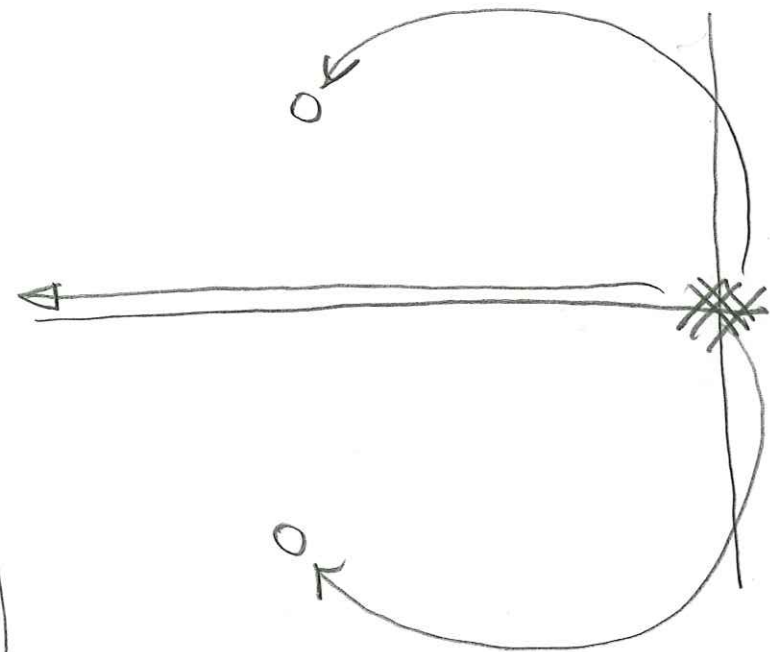
$$\Delta < 0 \rightarrow 2 \text{ Complex Zero}$$



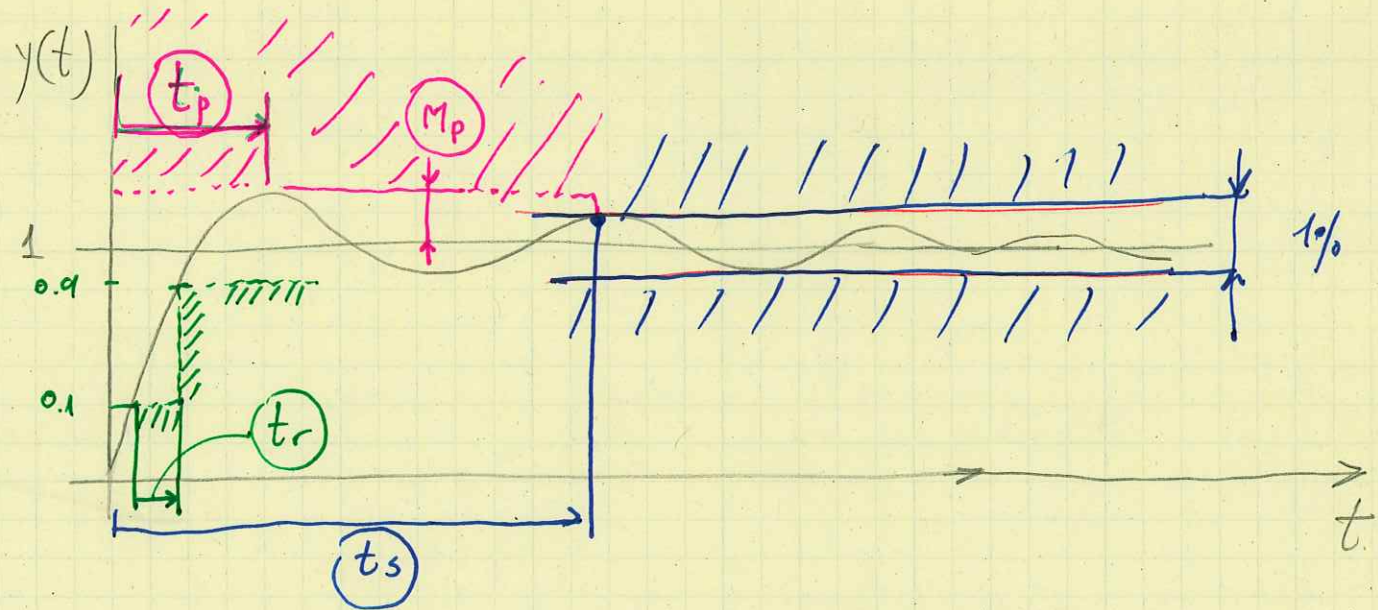
$$\Delta > 0 \Rightarrow \left(\frac{k_p}{k_d}\right)^2 > 4 \frac{k_I}{k_d}$$



$$\Delta < 0 \Rightarrow \left(\frac{k_p}{k_d}\right)^2 < 4 \frac{k_I}{k_d}$$



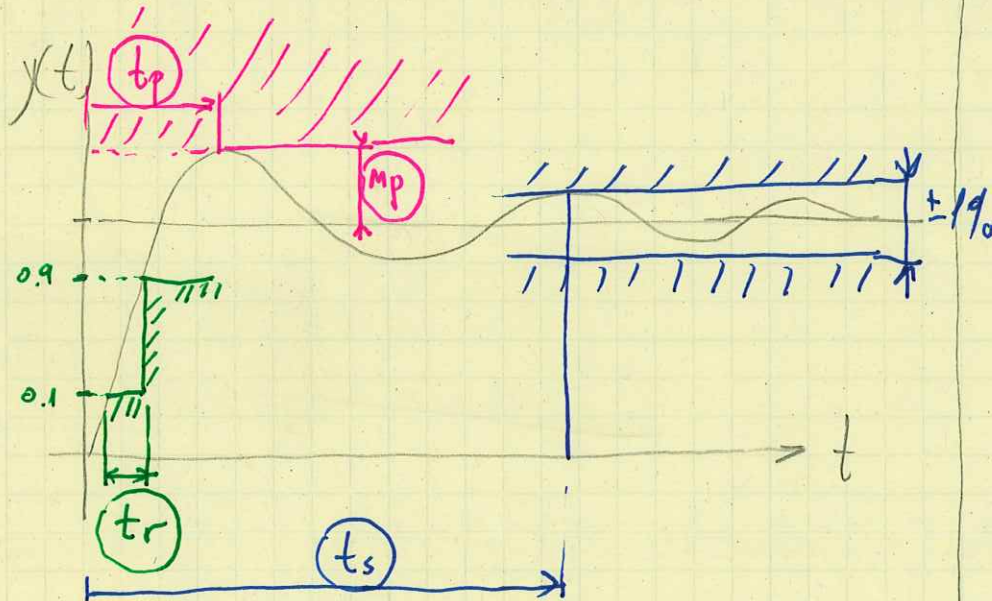
DESIGN - TIME DOMAIN SPECIFICATIONS



- RISE TIME (t_r) the time it takes the system to reach the vicinity of its new set point
- SETTING TIME (t_s) the time it takes the system transient to decay
- OVERSHOOT (M_p) - The ration between the maximal value and the final value(%)
- Peak time (t_p) - the time it takes the system to reach the maximum overshoot

DESIGN - TIME DOMAIN / FREQUENCY DOMAIN

TIME DOMAIN



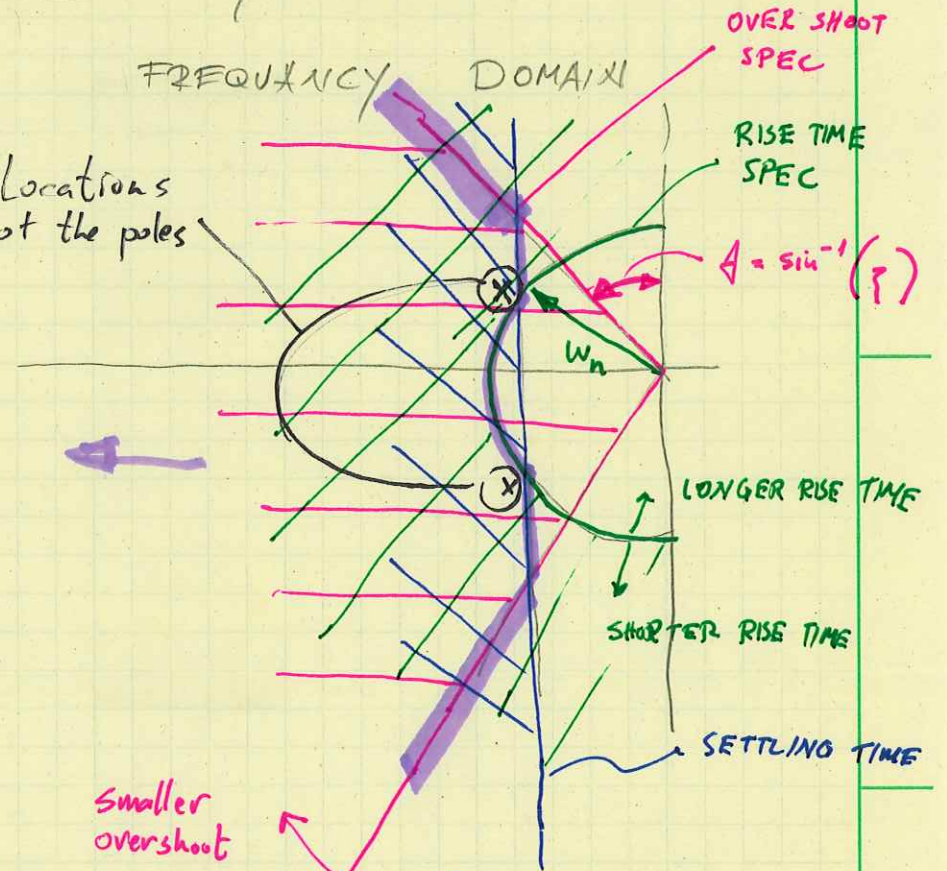
$$① \quad t_r \rightarrow \omega_n \geq \frac{1.8}{t_r}$$

$$② \quad M_p \rightarrow \zeta \geq \zeta(M_p) \quad \text{Graph}$$

$$③ \quad \Delta \rightarrow \Delta \geq \frac{4.6}{t_s}$$

FREQUENCY DOMAIN

Locations of the poles



Smaller overshoot

Larger overshoot

SHORTER SETTLING TIME

LONGER SETTLING TIME

