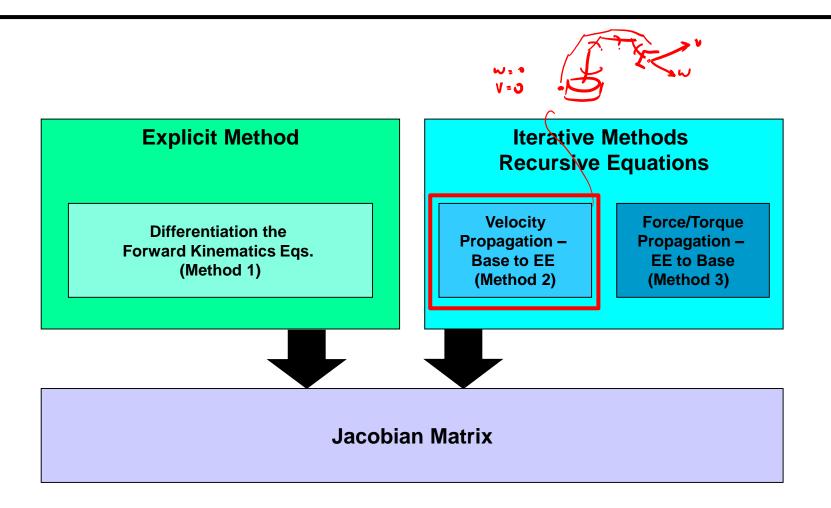


Jacobian Iterative Method -Velocity Propagation (Method No. 2) Part 1 – Method Derivation





Jacobian Matrix - Derivation Methods

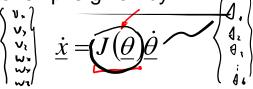






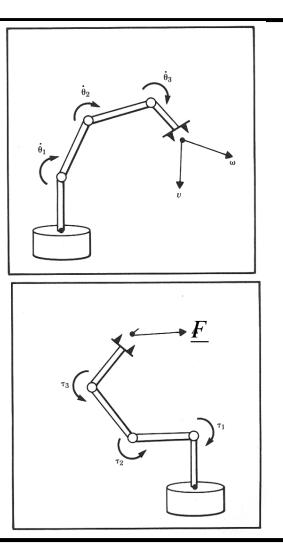
Jacobian Matrix - Introduction

• In the field of robotics the Jacobian matrix describe the relationship between the joint angle rates $(\underline{\dot{\theta}}_N)$ and the translation and rotation velocities of the end effector $(\underline{\dot{x}})$. This relationship is given by:



In addition to the velocity relationship, we are also interested in developing a relationship between the robot joint torques (<u>τ</u>) and the forces and moments (<u>F</u>) at the robot end effector (Static Conditions). This relationship is given by:

$$\underline{\tau} = J(\underline{\theta})^T \underline{F}$$







Summary – Changing Frame of Representation

- Linear and Rotational Velocity
 - Vector Form

$${}^{A}V_{Q} = {}^{A}V_{BORG} + {}^{A}_{B}R^{B}V_{Q} + {}^{A}\Omega_{B} \times {}^{A}_{B}R^{B}P_{Q}$$

– Matrix Form

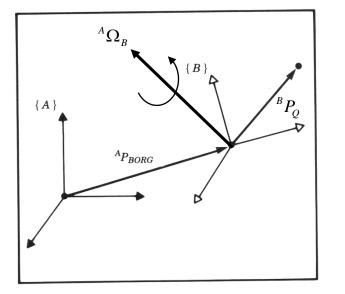
$${}^{A}V_{Q} = {}^{A}V_{BORG} + {}^{A}_{B}R^{B}V_{Q} + {}^{A}_{B}\dot{R}_{\Omega}\left({}^{A}_{B}R^{B}P_{Q}\right)$$

• Angular Velocity

- Vector Form
- Matrix Form
$$A \Omega_{C} = {}^{A} \Omega_{B} + {}^{A}_{B} R^{B} \Omega_{C}$$

$$A \Omega_{C} = {}^{A} \Omega_{B} + {}^{A}_{B} R^{B} \Omega_{C}$$

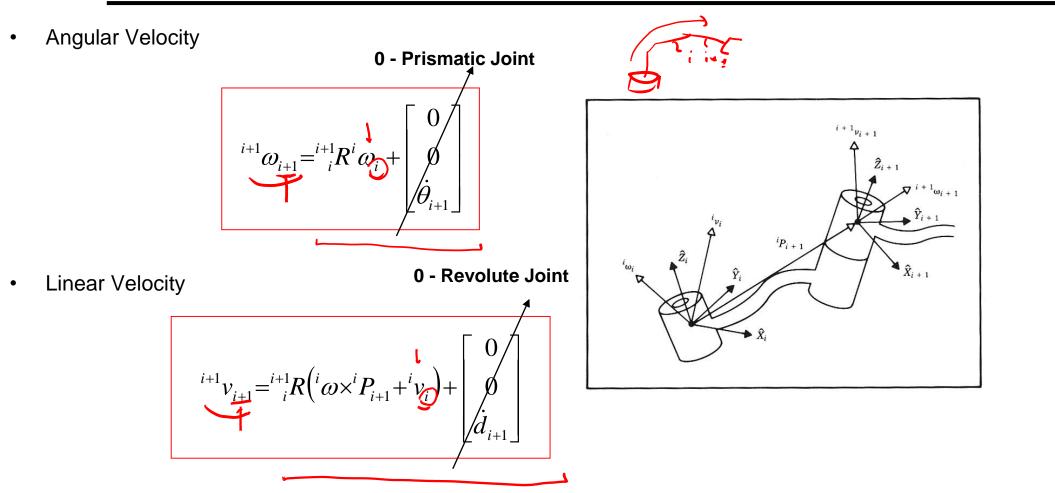
$$A \Omega_{C} = {}^{A} \Omega_{B} + {}^{A}_{B} R^{B} \Omega_{C}$$







Velocity of Adjacent Links - Summary







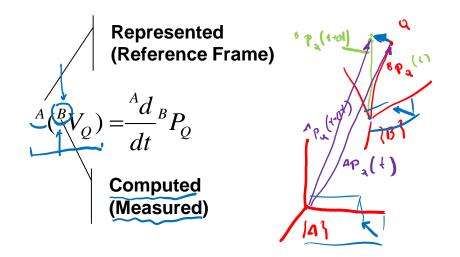
Representation / Reference Frame Computed / Measured Frame

Frame Notation





- As with any vector, a velocity vector may be described in terms of any frame, and this frame of reference is noted with a leading superscript.
- A velocity vector **<u>computed</u>** in frame {B} and **<u>represented</u>** in frame {A} would be written







- The homogeneous transform matrix provides a complete description of the linear and angular position relationship between adjacent links.
- These descriptions may be combined together to describe the position of a link relative to the robot base frame {0}.

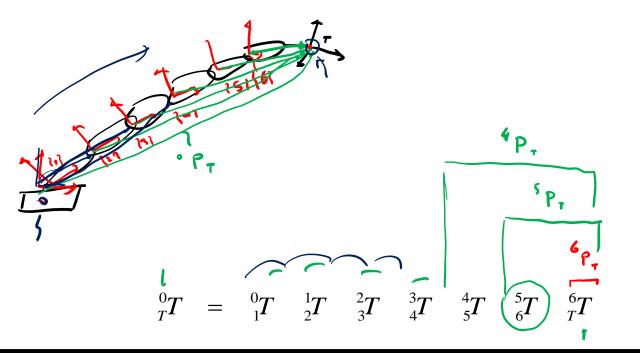
 $_{i}^{o}T = _{1}^{o}T _{2}^{1}T \cdots _{i}^{i-1}T$

• A similar description of the linear and angular velocities between adjacent links as well as the base frame would also be useful.





Position Propagation







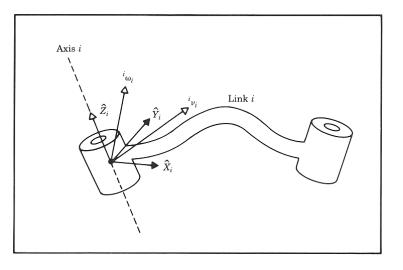
- In considering the motion of a robot link we will always use link frame {0} as the reference frame (Computed AND Represented). However any frame can be used as the reference (represented) frame including the link's own frame (*i*)
 - Where: v_i is the linear velocity of the origin of link frame (*i*) with respect to frame {0} (Computed AND Represented)
 - ω_i is the angular velocity of the origin of link frame (*i*) with respect to frame {0} (Computed AND Represented)
- Expressing the velocity of a frame {*i*} (associated with link *i*) relative to the robot base (frame {0}) using our previous notation is defined as follows:

$$= \underbrace{v_i}_{i} = \underbrace{v_i}_{i} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$
$$= \underbrace{\omega_i}_{i} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$





• The velocities differentiate (computed) relative to the base frame $\{0\}$ are often represented relative to other frames $\{k\}$. The following notation is used for this conditions



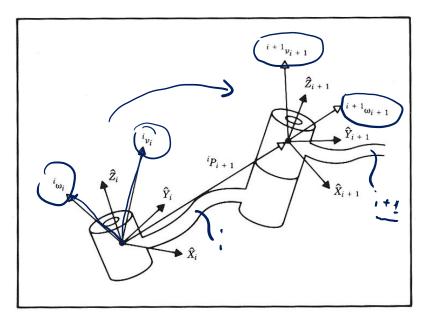




Velocity Propagation

- Given: A manipulator A chain of rigid bodies each one capable of moving relative to its neighbor
- Problem: Calculate the linear and angular velocities of the link of a robot
- Solution (Concept): Due to the robot structure (serial mechanism) we can compute the velocities of each link in order starting from the base.

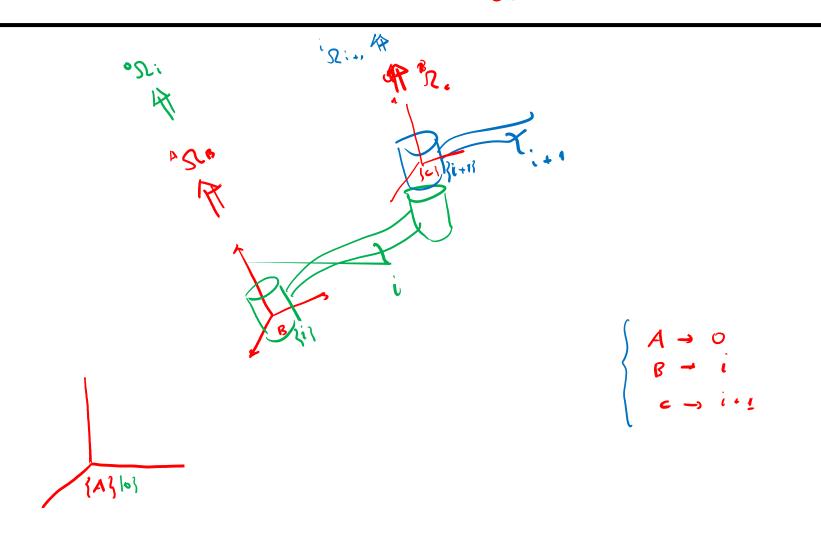
The velocity of link i+1 will be that of link i, plus whatever new velocity components were added by joint i+1







Velocity of Adjacent Links - Angular Velocity 0/5







Angular Velocity Propagation





Velocity of Adjacent Links - Angular Velocity 1/5

• From the relationship developed previously

$$\rightarrow {}^{A}\Omega_{C} = {}^{A}\Omega_{B} + {}^{A}_{B}R^{B}\Omega_{C}$$

• we can re-assign link names to calculate the velocity of any link *i* relative to the base frame {0}





 ${}^{i+1}_{0}R^{0}\Omega_{i+1} = {}^{i+1}_{0}R^{0}\Omega_{i} + {}^{i+1}_{0}R^{0}_{i}R^{i}\Omega_{i+1}$

• Using the recently defined notation, we have

$$\omega_{i+1} = \omega_{i+1} = \omega_i + \omega_i + \omega_i + \omega_i + \omega_i + \omega_i + \omega_i$$

^{*i*+1} ω_{i+1} - Angular velocity of frame {*i*+1} measured relative to the robot base, and expressed in frame {*i*+1} - **Recall the car example** ${}^{c} [{}^{w}V_{c}] = {}^{c}V_{c}$ - Angular velocity of frame {*i*} measured relative to the robot base, and expressed in frame {*i*+1} ${}^{i+1}R^{i}\Omega_{i+1}$ - Angular velocity of frame {*i*+1} measured relative to frame {*i*} and

expressed in frame {*i*+1}





Velocity of Adjacent Links - Angular Velocity 3/5

$${}^{i+1}\omega_{i+1} = {}^{i+1}\omega_i + {}^{i+1}R^i\Omega_{i+1}$$

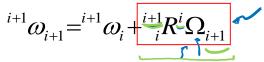
• Angular velocity of frame $\{i\}$ measured relative to the robot base, expressed in frame $\{i+1\}$

 $^{i+1}\omega_i = {}^{i+1}_{i}R^i\omega_i$

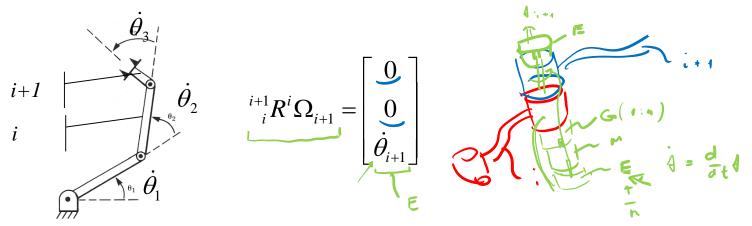




Velocity of Adjacent Links - Angular Velocity 4/5



- Angular velocity of frame {*i*+1} measured (differentiate) in frame {*i*} and represented (expressed) in frame {*i*+1}
- Assuming that a joint has only 1 DOF. The joint configuration can be either revolute joint (*angular velocity*) or prismatic joint (Linear velocity).
- Based on the frame attachment convention in which we assign the Z axis pointing along the *i*+1 joint axis such that the two are coincide (rotations of a link is preformed only along its Z- axis) we can rewrite this term as follows:







• The result is a *recursive equation* that shows the angular velocity of one link in terms of the angular velocity of the previous link plus the relative motion of the two links.

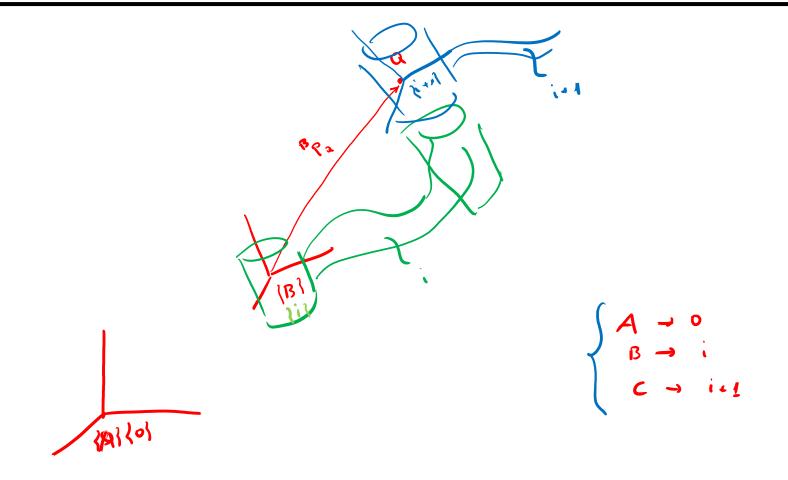
$$\begin{bmatrix} i^{i+1}\omega_{i+1} = i^{i+1}R^{i}\omega_{i} + \begin{bmatrix} 0\\0\\\dot{\theta}_{i+1} \end{bmatrix}$$

• Since the term ${}^{i+1}\omega_{i+1}$ depends on all previous links through this recursion, the angular velocity is said to propagate from the base to subsequent links.





Velocity of Adjacent Links - Linear Velocity 0/6







Linear Velocity Propagation





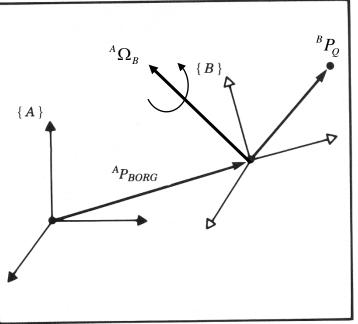
Velocity of Adjacent Links - Linear Velocity 1/6

- Simultaneous Linear and Rotational Velocity
- The derivative of a vector in a moving frame (linear and rotation velocities) as seen from a stationary frame
- Vector Form

$${}^{A}V_{Q} = {}^{A}V_{BORG} + {}^{A}_{B}R^{B}V_{Q} + {}^{A}\Omega_{B} \times {}^{A}_{B}R^{B}P_{Q}$$

Matrix Form

$${}^{A}V_{Q} = {}^{A}V_{BORG} + {}^{A}_{B}R^{B}V_{Q} + {}^{A}_{B}\dot{R}_{\Omega}\left({}^{A}_{B}R^{B}P_{Q}\right)$$







• From the relationship developed previously (matrix form)

$${}^{A}V_{Q} = {}^{A}V_{BORG} + {}^{A}_{B}R^{B}V_{Q} + {}^{A}_{B}\dot{R}_{\Omega}\left({}^{A}_{B}R^{B}P_{Q}\right)$$

we re-assign link frames for adjacent links (*i* and *i* +1) with the velocity computed relative to the robot base frame {0}

$$\begin{cases} A \to 0 \\ B \to i \\ C \to i+1 \end{cases}$$

$${}^{0}V_{i+1} = {}^{0}_{i}\dot{R}_{\Omega} \left({}^{0}_{i}R^{i}P_{i+1} \right) + {}^{0}V_{i} + {}^{0}_{i}R^{i}V_{i+1}$$

• By pre-multiplying both sides of the equation by ${}^{i+1}_{0}R$, we can convert the frame of reference for the left side to frame {*i*+1}





$${}^{i+1}_{0}R^{0}V_{i+1} = {}^{i+1}_{0}R^{0}_{i}\dot{R}_{\Omega} \left({}^{0}_{i}R^{i}P_{i+1} \right) + {}^{i+1}_{0}R^{0}V_{i} + {}^{i+1}_{0}R^{0}_{i}R^{i}V_{i+1}$$

• Which simplifies to

$${}^{i+1}_{0}R^{0}V_{i+1} = {}^{i+1}_{0}R^{0}_{i}\dot{R}_{\Omega} \left({}^{0}_{i}R^{i}P_{i+1} \right) + {}^{i+1}_{0}R^{0}V_{i} + {}^{i+1}_{i}R^{i}V_{i+1}$$

• Factoring out ${}^{i+1}_{i}R$ from the left side of the first two terms

$${}^{i+1}_{0}R^{0}V_{i+1} = {}^{i+1}_{i}R\left({}^{i}_{0}R^{0}_{i}\dot{R}^{0}_{\Omega i}R^{i}P_{i+1} + {}^{i}_{0}R^{0}V_{i}\right) + {}^{i+1}_{i}R^{i}V_{i+1}$$





Velocity of Adjacent Links - Linear Velocity 4/6

$${}^{i+1}_{0}R^{0}V_{i+1} = {}^{i+1}_{i}R \Big({}^{i}_{0}R^{0}_{i}\dot{R}^{0}_{\Omega i}R^{i}P_{i+1} + {}^{i}_{0}R^{0}V_{i} \Big) + \underbrace{{}^{i+1}_{i}R^{i}_{V_{i+1}}}_{i} + \underbrace{{}^{i}_{i}R^{0}_{i}V_{i}}_{i} \Big) + \underbrace{{}^{i+1}_{i}R^{i}_{V_{i+1}}}_{i} + \underbrace{{}^{i}_{i}R^{0}_{i}V_{i}}_{i} \Big) + \underbrace{{}^{i+1}_{i}R^{i}_{V_{i+1}}}_{i} + \underbrace{{}^{i}_{i}R^{0}_{i}V_{i}}_{i} \Big) + \underbrace{{}^{i+1}_{i}R^{i}_{i}V_{i+1}}_{i} + \underbrace{{}^{i}_{i}R^{0}_{i}V_{i}}_{i} \Big) + \underbrace{{}^{i+1}_{i}R^{i}_{i}V_{i}}_{i} + \underbrace{{}^{i}_{i}R^{0}_{i}V_{i}}_{i} \Big) + \underbrace{{}^{i+1}_{i}R^{i}_{i}V_{i}}_{i} + \underbrace{{}^{i}_{i}R^{0}_{i}V_{i}}_{i} \Big) + \underbrace{{}^{i}_{i}R^{i}_{i}V_{i}}_{i} + \underbrace{{}^{i}_{i}R^{i}_{i}V_{i}}_{i} + \underbrace{{}^{i}_{i}R^{i}_{i}V_{i}}_{i} + \underbrace{{}^{i}_{i}R^{i}_{i}V_{i}}_{i} + \underbrace{{}^{i}_{i}R^{i}V_{i}}_{i} + \underbrace{{}^{i}_{i}R^{i}_{i}V_{i}}_{i} + \underbrace{{}^{i}_{i}R^{i}_{i}V_{i}}_{i} + \underbrace{{}^{i}_{i}R^{i}V_{i}}_{i} + \underbrace{{}^{i}_{i}R^{i}V_$$

 ${}^{i+1}_{i}R^{i}V_{i+1}$ - Linear velocity of frame $\{i+1\}$ measured relative to frame $\{i\}$ and expressed in frame $\{i+1\}$

- Assuming that a joint has only 1 DOF. The joint configuration can be either revolute joint (angular velocity) or prismatic joint (Linear velocity).
- Based on the frame attachment convention in which we assign the Z axis pointing along the *i*+1 joint axis such that the two are coincide (translation of a link is preformed only along its Z- axis) we can rewrite this term as follows:

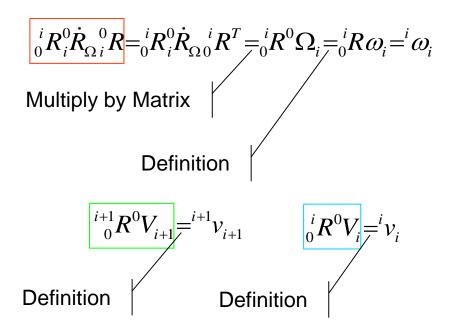
$${}^{i+1}_{i}R^{i}V_{i+1} = \begin{bmatrix} \underline{0} \\ \underline{0} \\ \dot{d}_{i+1} \end{bmatrix} \xrightarrow{\rho} \underbrace{(\mathbf{1} + \mathbf{1})}_{i}$$





Velocity of Adjacent Links - Linear Velocity 5/6

$$\begin{bmatrix} i+1\\0\\R^0V_{i+1} \end{bmatrix} = {}^{i+1}_{i}R\left({}^{i}_{0}R^{0}_{i}\dot{R}^{0}_{\Omega i}R^{i}P_{i+1} + {}^{i}_{0}R^{0}V_{i}\right) + \begin{bmatrix} 0\\0\\\dot{d}_{i+1} \end{bmatrix}$$





	Angular Velocity - Matri ${}^{A}V_{O} = {}^{A}V_{BORG} + {}^{A}R^{B}V_{O} + {}^{A}\Omega_{B} \times {}^{A}R^{B}P_{O}$ ${}^{A}V_{Q} =$	
	Matrix Form Ve	ector Form
Definition	${}^{A}_{B}\dot{R}_{\Omega} \equiv \begin{bmatrix} 0 & -\Omega_{z} & \Omega_{y} \\ \Omega_{z} & 0 & -\Omega_{x} \\ -\Omega_{y} & \Omega_{x} & 0 \end{bmatrix}$	$ \begin{bmatrix} A \\ \Omega_B \end{bmatrix} \begin{bmatrix} \Omega_x \\ \Omega_y \\ \Omega_z \end{bmatrix} $
Multiply by Constant	$k \begin{bmatrix} A \dot{R} \\ B \dot{R}_{\Omega} \end{bmatrix}$	$k \left[{}^{A}\Omega_{B} \right]$
Multiply by Vector	$\begin{bmatrix} {}^{A}_{B}\dot{R}_{\Omega}\end{bmatrix}\begin{bmatrix} x\\ y\\ z\end{bmatrix}$	${}^{A}\Omega_{B} \times \begin{bmatrix} x \\ y \\ z \end{bmatrix} \qquad \qquad$
	$\begin{bmatrix} {}^{s}R \\ {}^{t}R \end{bmatrix} \begin{bmatrix} {}^{A}\dot{R} \\ {}^{B}\dot{R} \\ {}^{\Omega} \end{bmatrix} \begin{bmatrix} {}^{s}R \\ {}^{T}R \end{bmatrix}$	${}^{T} \qquad \left[{}^{s}_{t} R \right] \left[{}^{A} \Omega_{B} \right]$
Multiply by Matrix		





 The result is a <u>recursive equation</u> that shows the linear velocity of one link in terms of the previous link plus the relative motion of the two links.

$$\stackrel{i+1}{\underset{i+1}{v_{i+1}}} = \stackrel{i+1}{\underset{i}{\overset{i}{R}}} \left(\stackrel{i}{\omega_{i}} \times \stackrel{i}{\underset{i+1}{v_{i+1}}} + \stackrel{i}{\underset{v_{i}}{v_{i}}} \right) + \begin{bmatrix} 0\\0\\\dot{d}_{i+1} \end{bmatrix}$$

• Since the term ${}^{i+1}V_{i+1}$ depends on all previous links through this recursion, the angular velocity is said to propagate from the base to subsequent links.

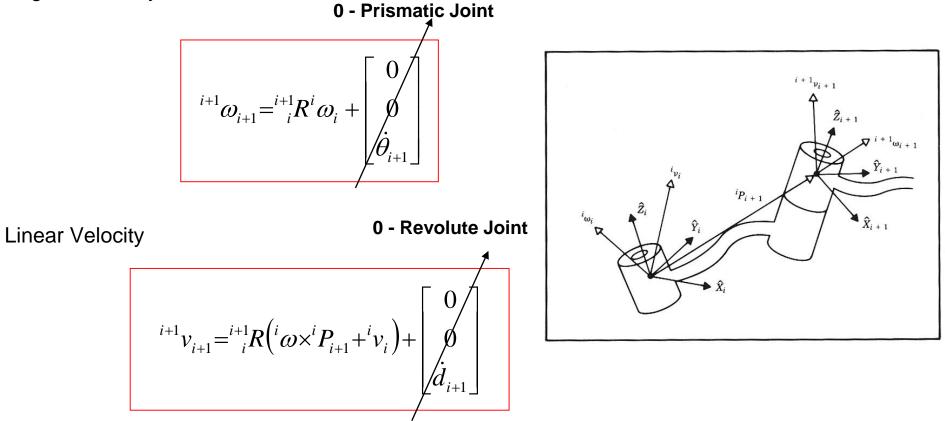




٠

Velocity of Adjacent Links - Summary

Angular Velocity







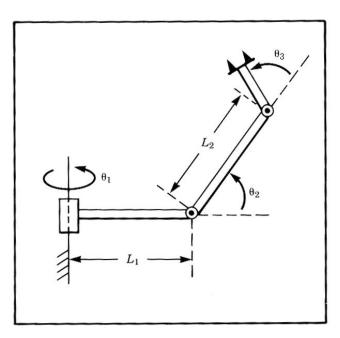
3R – Example

Analytical Approach





• For the manipulator shown in the figure, compute the angular and linear velocity of the "tool" frame relative to the base frame expressed in the "tool" frame (that is, calculate ${}^4\omega_4$ and 4v_4).

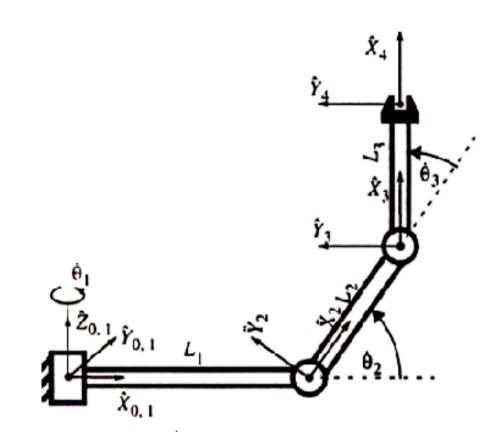






Angular and Linear Velocities - 3R Robot - Example

• Frame attachment

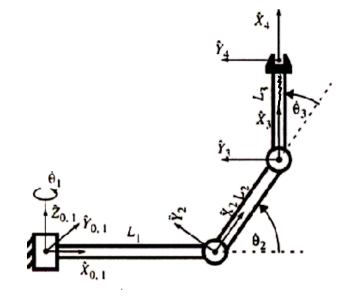






Angular and Linear Velocities - 3R Robot - Example

• DH Parameters

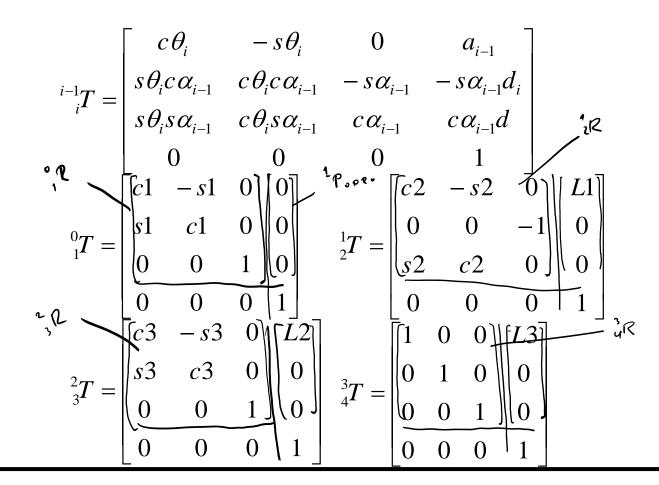


	i	α_{i-1}	a_{i-1}	d_i	$ heta_i$
	1	0	0	0	θ_1
	2	90	L1	0	θ_2
	3	0	L2	0	θ_3
Ī	4	0	L3	0	0





• From the DH parameter table, we can specify the homogeneous transform matrix for each adjacent link pair:





• Compute the angular velocity of the end effector frame relative to the base frame expressed at the end effector frame.

$$^{i+1}\omega_{i+1} = {}^{i+1}_{i}R^{i}\omega_{i} + \begin{bmatrix} 0\\0\\\dot{\theta}_{i+1}\end{bmatrix}$$

• For *i=0*

$${}^{1}\omega_{1} = {}^{1}_{0}R^{0}\omega_{0} + \begin{bmatrix} 0\\0\\\dot{\theta}_{1} \end{bmatrix} = \begin{bmatrix} c1 & s1 & 0\\-s1 & c1 & 0\\0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0\\0\\0\\\dot{\theta}_{1} \end{bmatrix} + \begin{bmatrix} 0\\0\\\dot{\theta}_{1} \end{bmatrix} = \begin{bmatrix} 0\\0\\\dot{\theta}_{1} \end{bmatrix}$$



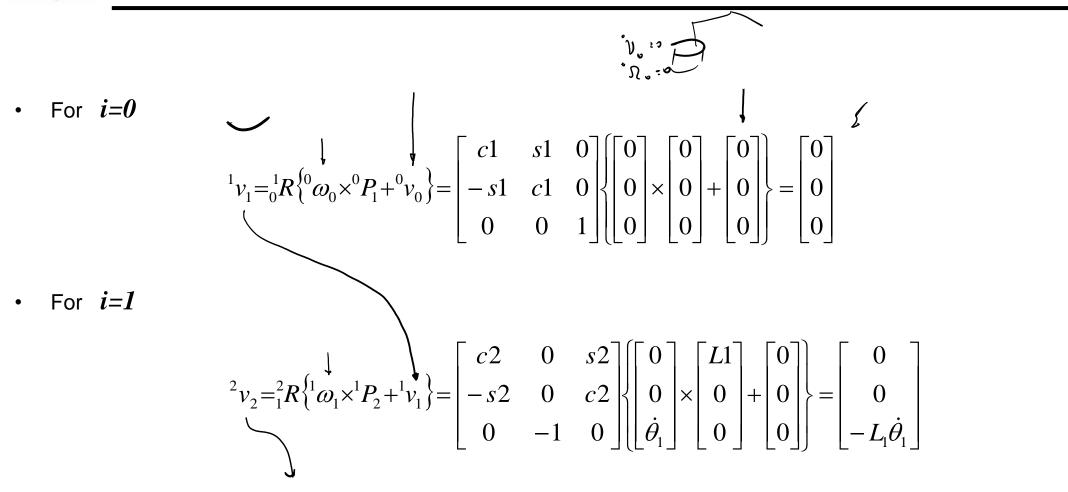




- Compute the linear velocity of the end effector frame relative to the base frame expressed at the end effector frame.
- •
- Note that the term involving the prismatic joint has been dropped from the equation (it is equal to zero).

$${}^{i+1}v_{i+1} = {}^{i+1}_{i}R(i\omega \times {}^{i}P_{i+1} + {}^{i}v_i) + \begin{bmatrix} 0\\ 0\\ d_{i+1} \end{bmatrix}$$









UCLA

• For *i=3*

$$= \begin{bmatrix} c3 & s3 & 0 \\ -s3 & c30 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{cases} s2\dot{\theta}_{1} \\ c2\dot{\theta}_{1} \\ \dot{\theta}_{2} \end{bmatrix} \times \begin{bmatrix} L2 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ -L1\dot{\theta}_{1} \end{bmatrix}$$
$$= \begin{bmatrix} c3 & s3 & 0 \\ -s3 & c3 & 0 \\ 0 & 0 & 1 \end{bmatrix} \{ \begin{bmatrix} 0 \\ L2\dot{\theta}_{1} \\ -L2c2\dot{\theta}_{1} - L1\dot{\theta}_{1} \end{bmatrix} \} = \begin{bmatrix} L2s3\dot{\theta}_{2} \\ L2c3\dot{\theta}_{2} \\ (-L1 - L2c2)\dot{\theta}_{1} \end{bmatrix}$$



• For *i=4*

$$\int_{4}^{4} v_{4} = {}_{3}^{4} R \{ {}^{3} \omega_{3} \times {}^{3} P_{4} + {}^{3} v_{3} \} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \left\{ \begin{bmatrix} s 2 3 \dot{\theta}_{1} \\ c 2 3 \dot{\theta}_{1} \\ \dot{\theta}_{2} + \dot{\theta}_{3} \end{bmatrix} \times \begin{bmatrix} L 3 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} L 2 s 3 \dot{\theta}_{2} \\ (-L 1 - L 2 c 2) \dot{\theta}_{1} \end{bmatrix} \right\}$$
$$= \begin{bmatrix} L 2 s 3 \dot{\theta}_{2} \\ (L 2 c 3 + L 3) \dot{\theta}_{2} + L 3 \dot{\theta}_{3} \\ (-L 1 - L 2 c 2 - L 3 c 2 3) \dot{\theta}_{1} \end{bmatrix}$$



- Note that the linear and angular velocities (${}^4\omega_4$, 4v_4) of the end effector where differentiate (measured) in frame {0} however represented (expressed) in frame {4}
- In the car example: Observer sitting in the "Car" ${}^{C}[{}^{W}V_{C}]$ Observer sitting in the "World" ${}^{W}[{}^{W}V_{C}]$

$${}^{k}v_{i} \equiv {}^{k} \begin{bmatrix} {}^{0}V_{i} \end{bmatrix} = {}^{k}_{0}R \begin{bmatrix} {}^{0}V_{i} \end{bmatrix} = {}^{k}_{0}R \cdot v_{i}$$
$${}^{k}\omega_{i} \equiv {}^{k} \begin{bmatrix} {}^{0}\Omega_{i} \end{bmatrix} = {}^{k}_{0}R \begin{bmatrix} {}^{0}\Omega_{i} \end{bmatrix} = {}^{k}_{0}R \cdot \omega_{i}$$

Solve for v_4 and ω_4 by multiply both side of the questions from the left by ${}^4_0 R^{-1}$

$${}^{4}v_{4} = {}^{4}_{0}R \cdot v_{4}$$
$${}^{4}\omega_{4} = {}^{4}_{0}R \cdot \omega_{4}$$



• Multiply both sides of the equation by the inverse transformation matrix, we finally get the linear and angular velocities expressed and measured in the stationary frame {0}

$$v_{4} = {}_{0}^{4}R^{-1} \cdot {}^{4}v_{4} = {}_{0}^{4}R^{T} \cdot {}^{4}v_{4} = {}_{4}^{0}R \cdot {}^{4}v_{4}$$
$$\omega_{4} = {}_{0}^{4}R^{-1} \cdot {}^{4}\omega_{4} = {}_{0}^{4}R^{T} \cdot {}^{4}\omega_{4} = {}_{4}^{0}R \cdot {}^{4}\omega_{4}$$
$${}^{0}_{4}T = {}_{1}^{0}T {}_{2}^{1}T {}_{3}^{2}T {}_{4}^{3}T$$





3R – Example

Analytical Approach – Graphical Interpretation





