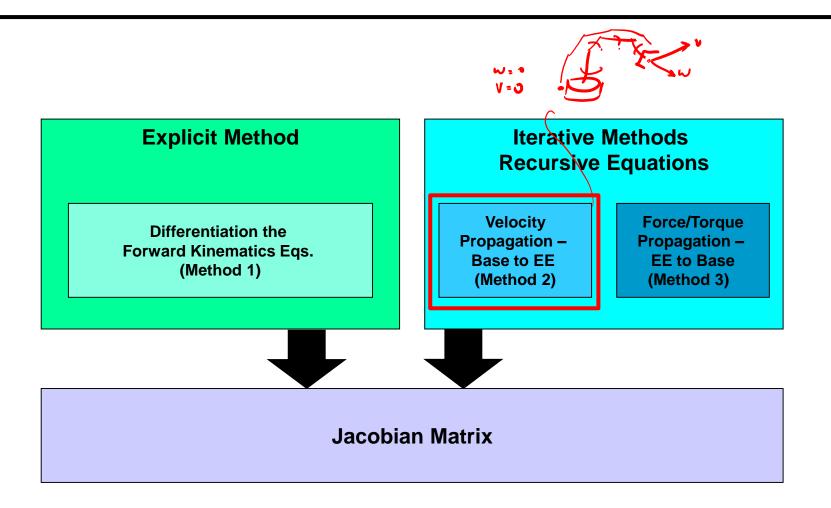


Jacobian Iterative Method -Velocity Propagation (Method No. 2) Part 1 – Method Derivation





Jacobian Matrix - Derivation Methods



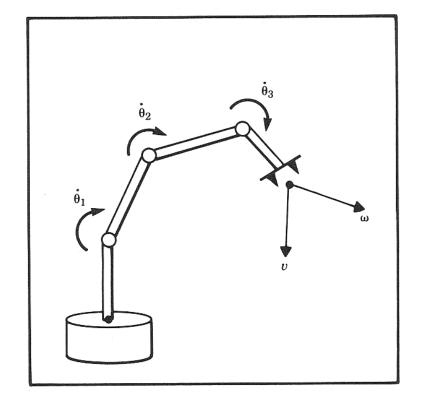




Jacobian Matrix - Introduction

 In the field of robotics the Jacobian matrix describe the relationship between the joint angle rates (<u>\u00f3</u>_N) and the translation and rotation velocities of the end effector (<u>\u00ex</u>). This relationship is given by:

 $\nu = \mathbf{J} (\Theta) \dot{\Theta}$ $\nu = \frac{d}{dt} [X] = \begin{bmatrix} \begin{bmatrix} v_N \\ \vdots \\ \omega_N \end{bmatrix} = \begin{bmatrix} v_X \\ v_y \\ \vdots \\ \omega_x \\ \omega_y \\ \omega_z \end{bmatrix}$ $\dot{\Theta} = \mathbf{J} (\underline{\theta})^{-1} \nu$







Summary – Changing Frame of Representation

- Linear and Rotational Velocity
 - Vector Form

$${}^{A}V_{Q} = {}^{A}V_{BORG} + {}^{A}_{B}R^{B}V_{Q} + {}^{A}\Omega_{B} \times {}^{A}_{B}R^{B}P_{Q}$$

- Matrix Form

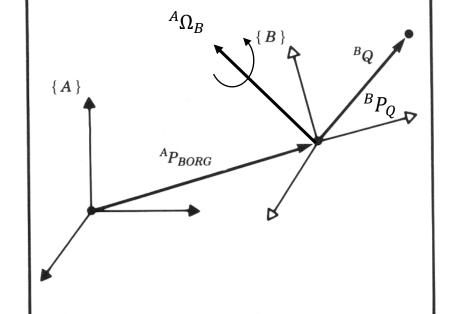
$${}^{A}V_{Q} = {}^{A}V_{BORG} + {}^{A}_{B}R{}^{B}V_{Q} + {}^{A}_{B}R_{\Omega}({}^{A}_{B}R{}^{B}P_{Q})$$

Angular Velocity

Vector Form

$${}^{A}\Omega_{C} = {}^{A}\Omega_{B} + {}^{A}_{B}R^{B}\Omega_{C}$$

Matrix Form
$$\dot{A}_{C}R_{\Omega} = \dot{A}_{B}R_{\Omega} + \dot{A}_{B}R_{C}^{B}R_{\Omega}A_{B}^{B}R^{T}$$



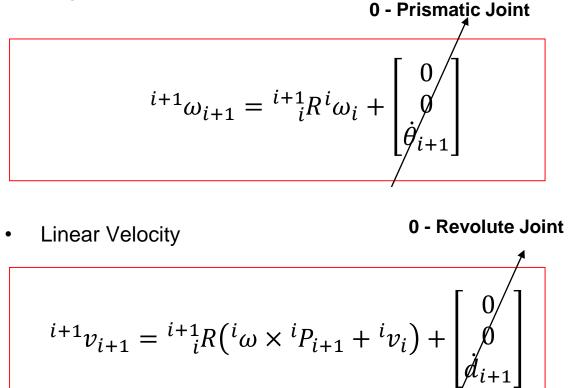


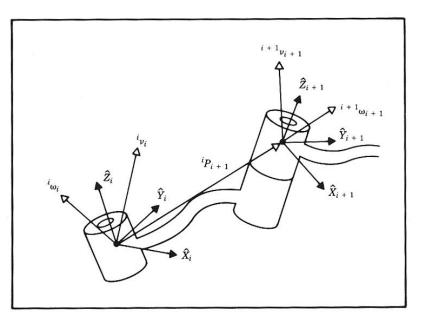


Velocity of Adjacent Links - Summary

 μ_{i+1}

Angular Velocity ٠









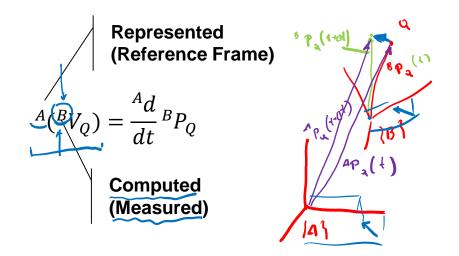
Representation / Reference Frame Computed / Measured Frame

Frame Notation





- As with any vector, a velocity vector may be described in terms of any frame, and this frame of reference is noted with a leading superscript.
- A velocity vector **<u>computed</u>** in frame {B} and **<u>represented</u>** in frame {A} would be written







- The homogeneous transform matrix provides a complete description of the linear and angular position relationship between adjacent links.
- These descriptions may be combined together to describe the position of a link relative to the robot base frame {0}.

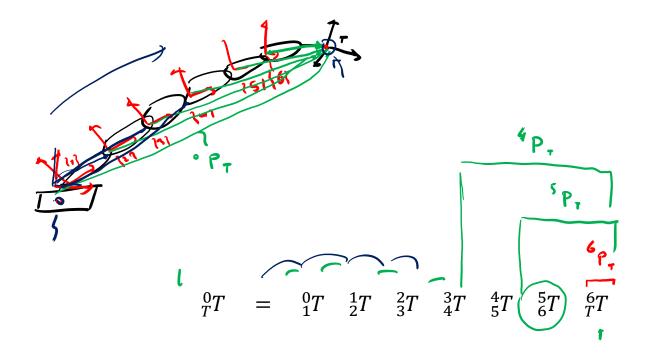
 ${}^{o}_{i}T = {}^{o}_{1}T {}^{1}_{2}T \cdots {}^{i-1}_{i}T$

• A similar description of the linear and angular velocities between adjacent links as well as the base frame would also be useful.





Position Propagation







- In considering the motion of a robot link we will always use link frame {0} as the reference frame (Computed AND Represented). However any frame can be used as the reference (represented) frame including the link's own frame (i)
 - Where: v_i is the linear velocity of the origin of link frame (*i*) with respect to frame {0} (Computed AND Represented)
 - ω_i is the angular velocity of the origin of link frame (*i*) with respect to frame {0} (Computed AND Represented)
- Expressing the velocity of a frame {*i*} (associated with link *i*) relative to the robot base (frame {0}) using our previous notation is defined as follows:

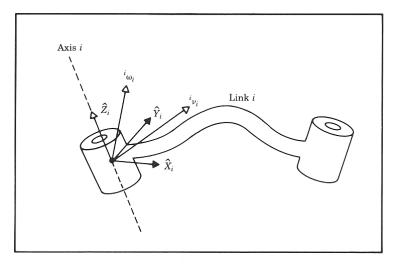
 $v_{i} \equiv {}^{0} \left[{}^{0}V_{i} \right] = \left[{}^{0}V_{i} \right]$ $\omega_{i} \equiv {}^{0} \left[{}^{0}\Omega_{i} \right] = \left[{}^{0}\Omega_{i} \right]$





• The velocities differentiate (computed) relative to the base frame $\{0\}$ are often represented relative to other frames $\{k\}$. The following notation is used for this conditions

$${}^{k}v_{i} \equiv {}^{k} \begin{bmatrix} {}^{0}V_{i} \end{bmatrix} = {}^{k}_{0}R \begin{bmatrix} {}^{0}V_{i} \end{bmatrix} = {}^{k}_{0}R \cdot v_{i}$$
$${}^{k}\omega_{i} \equiv {}^{k} \begin{bmatrix} {}^{0}\Omega_{i} \end{bmatrix} = {}^{k}_{0}R \begin{bmatrix} {}^{0}\Omega_{i} \end{bmatrix} = {}^{k}_{0}R \cdot \omega_{i}$$



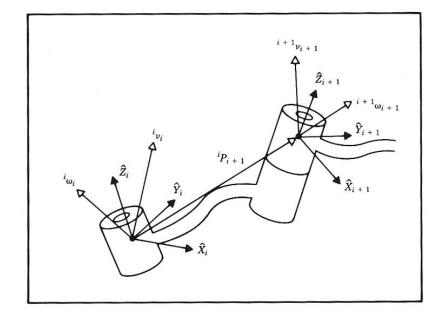




Velocity Propagation

- *Given:* A manipulator A chain of rigid bodies each one capable of moving relative to its neighbor
- Problem: Calculate the linear and angular velocities of the link of a robot
- Solution (Concept): Due to the robot structure (serial mechanism) we can compute the velocities of each link in order starting from the base.

The velocity of link i+1 will be that of link i, plus whatever new velocity components were added by joint i+1





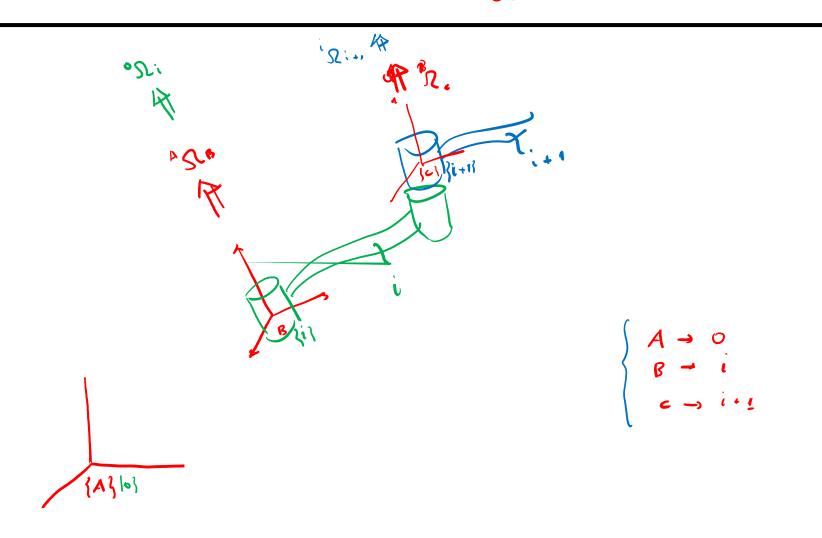


Angular Velocity Propagation





Velocity of Adjacent Links - Angular Velocity 0/5







• From the relationship developed previously

$${}^{A}\Omega_{C} = {}^{A}\Omega_{B} + {}^{A}_{B}R^{B}\Omega_{C}$$

• we can reassign link names to calculate the velocity of any link *i* relative to the base frame {0}

$$\begin{cases} A \to 0 \\ B \to i \\ C \to i+1 \end{cases}$$

$${}^{0}\Omega_{i+1} = {}^{0}\Omega_{i} + {}^{0}_{i}R^{i}\Omega_{i+1}$$

• We can convert the frame of reference from the base {0} to frame $\{i+1\}$ by pre-multiplying both sides of the equation by $i+_{0}^{1}R$, we can convert the frame of reference for the base {0} to frame $\{i+1\}$





$${}^{i+1}_{0}R^{0}\Omega_{i+1} = {}^{i+1}_{0}R^{0}\Omega_{i} + {}^{i+1}_{0}R^{0}_{i}R^{i}\Omega_{i+1}$$

• Using the recently defined notation, we have

$${}^{i+1}\omega_{i+1} = {}^{i+1}\omega_i + {}^{i+1}_i R^i \Omega_{i+1}$$

- ^{*i*+1} ω_{i+1} Angular velocity of frame {*i*+1} measured relative to the robot base, and expressed in frame {*i*+1} **Recall the car example** ${}^{c} [{}^{w}V_{c}] = {}^{c}v_{c}$
- $^{i+1}\omega_i$ Angular velocity of frame {*i*} measured relative to the robot base, and expressed in frame {*i*+1}

 ${}^{i+1}R{}^{i}\Omega_{i+1}$ - Angular velocity of frame $\{i+1\}$ measured relative to frame $\{i\}$ and expressed in frame $\{i+1\}$





Velocity of Adjacent Links - Angular Velocity 3/5

$${}^{i+1}\omega_{i+1} = {}^{i+1}\omega_i + {}^{i+1}_i R^i \Omega_{i+1}$$

• Angular velocity of frame $\{i\}$ measured relative to the robot base, expressed in frame $\{i+1\}$

$${}^{i+1}\omega_i = {}^{i+1}_i R^i \omega_i$$

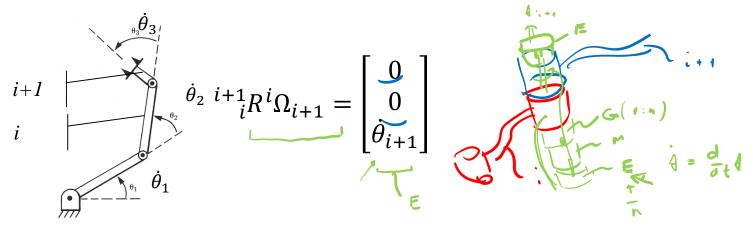




Velocity of Adjacent Links - Angular Velocity 4/5

$${}^{i+1}\omega_{i+1} = {}^{i+1}\omega_i + \underbrace{{}^{i+1}R^i\Omega_{i+1}}_{i}$$

- Angular velocity of frame {*i*+1} measured (differentiate) in frame {*i*} and represented (expressed) in frame {*i*+1}
- Assuming that a joint has only 1 DOF. The joint configuration can be either revolute joint (*angular velocity*) or prismatic joint (Linear velocity).
- Based on the frame attachment convention in which we assign the Z axis pointing along the *i*+1 joint axis such that the two are coincide (rotations of a link is preformed only along its Z- axis) we can rewrite this term as follows:







 The result is a <u>recursive equation</u> that shows the angular velocity of one link in terms of the angular velocity of the previous link plus the relative motion of the two links.

$${}^{i+1}\omega_{i+1} = {}^{i+1}_{i}R^{i}\omega_{i} + \begin{bmatrix} 0\\0\\\dot{\theta}_{i+1} \end{bmatrix}$$

• Since the term ${}^{i+1}\omega_{i+1}$ depends on all previous links through this recursion, the angular velocity is said to propagate from the base to subsequent links.



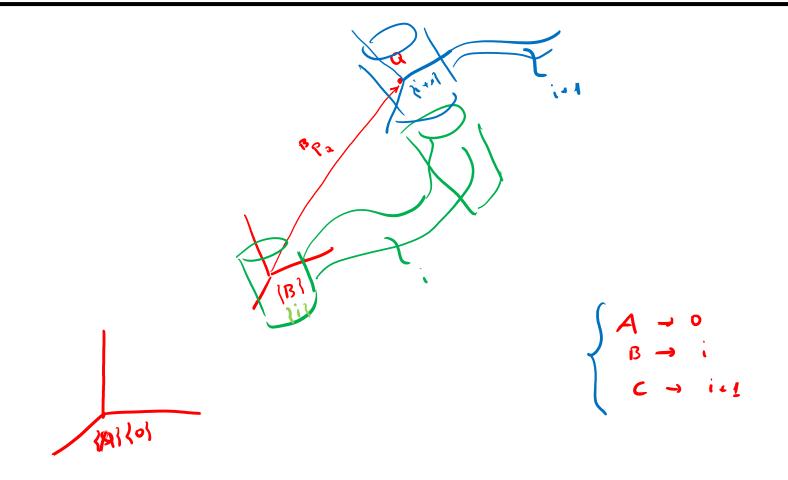


Linear Velocity Propagation





Velocity of Adjacent Links - Linear Velocity 0/6







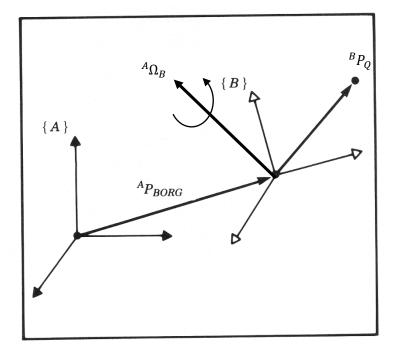
Velocity of Adjacent Links - Linear Velocity 1/6

- Simultaneous Linear and Rotational Velocity
- The derivative of a vector in a moving frame (linear and rotation velocities) as seen from a stationary frame
- Vector Form

$${}^{A}V_{Q} = {}^{A}V_{BORG} + {}^{A}_{B}R^{B}V_{Q} + {}^{A}\Omega_{B} \times {}^{A}_{B}R^{B}P_{Q}$$

• Matrix Form

$${}^{A}V_{Q} = {}^{A}V_{BORG} + {}^{A}_{B}R^{B}V_{Q} + {}^{A}_{B}R_{\Omega}({}^{A}_{B}R^{B}P_{Q})$$







• From the relationship developed previously (matrix form)

$${}^{A}V_{Q} = {}^{A}V_{BORG} + {}^{A}_{B}R^{B}V_{Q} + {}^{\dot{A}}_{B}R_{\Omega}({}^{A}_{B}R^{B}P_{Q})$$

we re-assign link frames for adjacent links (*i* and *i* +1) with the velocity computed relative to the robot base frame {0}

$$\begin{cases} A \to 0 \\ B \to i \\ C \to i+1 \end{cases}$$

$${}^{0}V_{i+1} = {}^{0}_{i} R_{\Omega} ({}^{0}_{i} R^{i} P_{i+1}) + {}^{0}V_{i} + {}^{0}_{i} R^{i} V_{i+1}$$

• We can convert the frame of reference from frame {0} to frame $\{i+1\}$ by pre-multiplying both sides of the equation by ${}^{i+1}R$





$${}^{i+1}_{0}R^{0}V_{i+1} = {}^{i+1}_{0}R^{0}_{i}R_{0}({}^{0}_{i}R^{i}P_{i+1}) + {}^{i+1}_{0}R^{0}V_{i} + {}^{i+1}_{0}R^{0}_{i}R^{i}V_{i+1}$$

• Which simplifies to

$${}^{i+1}_{0}R^{0}V_{i+1} = {}^{i+1}_{0}R^{i}_{i}R_{\Omega}({}^{0}_{i}R^{i}P_{i+1}) + {}^{i+1}_{0}R^{0}V_{i} + {}^{i+1}_{i}R^{i}V_{i+1}$$

• Factoring out ${}^{i+1}_{iR}$ from the blue term

$${}^{i+1}_{0}R^{0}V_{i+1} = {}^{i+1}_{i}R\left({}^{i}_{0}R^{0}_{i}R^{0}_{i}R^{i}P_{i+1} + {}^{i}_{0}R^{0}V_{i}\right) + {}^{i+1}_{i}R^{i}V_{i+1}$$





$${}^{i+1}_{0}R^{0}V_{i+1} = {}^{i+1}_{i}R\left({}^{i}_{0}R^{0}_{i}R^{0}_{i}R^{0}P_{i+1} + {}^{i}_{0}R^{0}V_{i}\right) + {}^{i+1}_{i}R^{i}_{i}V_{i+1}$$

 $i+1_i R^i V_{i+1}$ - Linear velocity of frame $\{i+1\}$ measured relative to frame $\{i\}$ and expressed in frame $\{i+1\}$

- Assuming that a joint has only 1 DOF. The joint configuration can be either revolute joint (angular velocity) or prismatic joint (Linear velocity).
- Based on the frame attachment convention in which we assign the Z axis pointing along the *i*+1 joint axis such that the two are coincide (translation of a link is preformed only along its Z- axis) we can rewrite this term as follows:

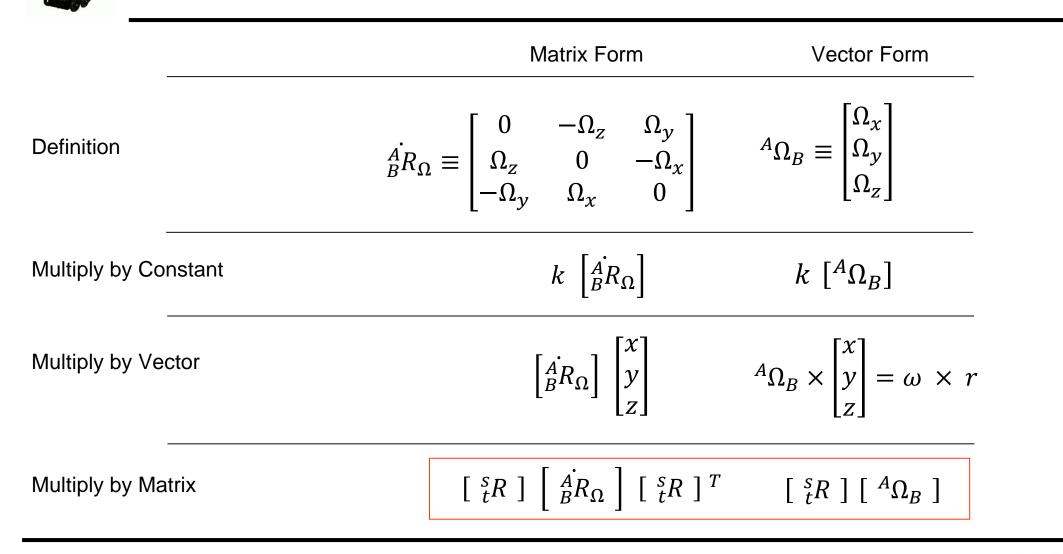
$${}^{i+1}_{i}R^{i}V_{i+1} = \begin{bmatrix} 0\\ 0\\ \dot{d}_{i+1} \end{bmatrix} \stackrel{\text{p}}{\underset{i=1}{\overset{i=1}{$$



$${}^{A}V_{Q} = {}^{A}V_{BORG} + {}^{A}_{B}R {}^{B}V_{Q} + {}^{A}\Omega_{B} \times {}^{A}_{B}R {}^{B}P_{Q}$$

 ${}^{A}V_{Q} = {}^{A}V_{BORG} + {}^{A}_{B}R {}^{B}V_{Q} + {}^{A}_{B}R_{\Omega} \left({}^{A}_{B}R {}^{B}P_{Q} \right)$

Angular Velocity - Matrix & Vector Forms



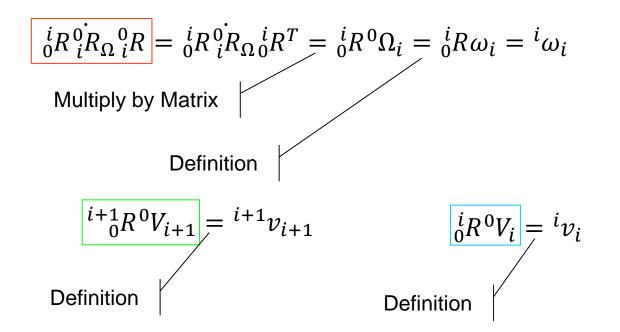
Instructor: Jacob Rosen Advanced Robotic - MAE 263 - Department of Mechanical & Aerospace Engineering - UCLA





Velocity of Adjacent Links - Linear Velocity 5/6

$$\stackrel{i+1}{_{0}}R^{0}V_{i+1} = \stackrel{i+1}{_{i}}R\left(\stackrel{i}{_{0}}R^{i}_{i}R_{\Omega}^{0}_{i}R^{i}P_{i+1} + \stackrel{i}{_{0}}R^{0}V_{i}\right) + \begin{bmatrix} 0\\0\\\dot{d}_{i+1}\end{bmatrix}$$







 The result is a <u>recursive equation</u> that shows the linear velocity of one link in terms of the previous link plus the relative motion of the two links.

$${}^{i+1}v_{i+1} = {}^{i+1}_{i}R({}^{i}\omega_i \times {}^{i}P_{i+1} + {}^{i}v_i) + \begin{bmatrix} 0\\0\\\dot{d}_{i+1}\end{bmatrix}$$

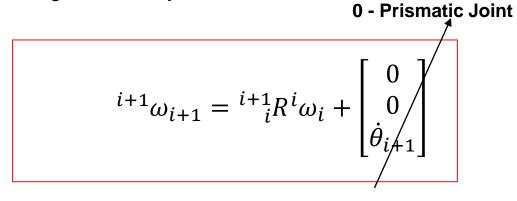
• Since the term ${}^{i+1}v_{i+1}$ depends on all previous links through this recursion, the angular velocity is said to propagate from the base to subsequent links.





Velocity of Adjacent Links - Summary

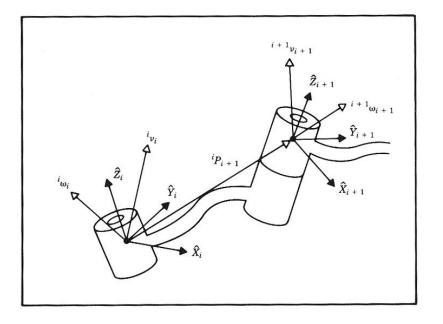
Angular Velocity



Linear Velocity

0 - Revolute Joint

$${}^{i+1}v_{i+1} = {}^{i+1}_{i}R(i\omega \times {}^{i}P_{i+1} + {}^{i}v_i) + \begin{bmatrix} 0\\0\\\dot{d}_{i+1}\end{bmatrix}$$







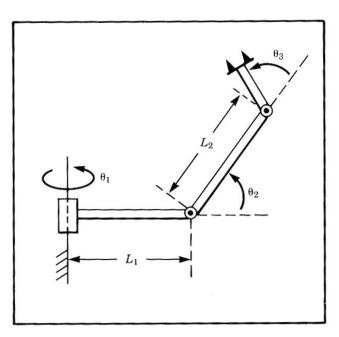
3R – Example

Analytical Approach





• For the manipulator shown in the figure, compute the angular and linear velocity of the "tool" frame relative to the base frame expressed in the "tool" frame (that is, calculate ${}^4\omega_4$ and 4v_4).

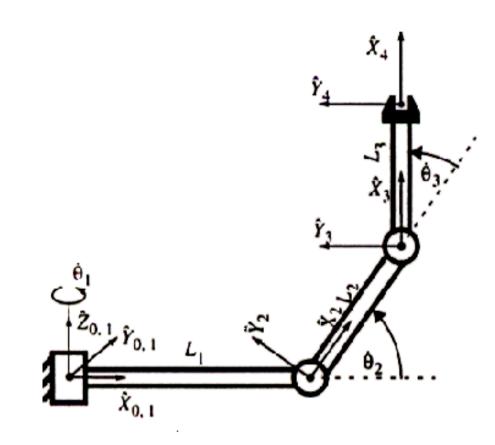






Angular and Linear Velocities - 3R Robot - Example

• Frame attachment

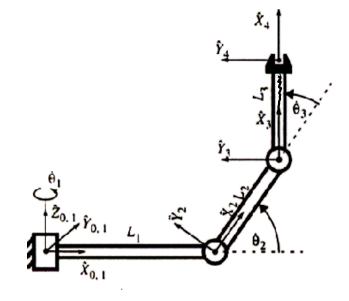






Angular and Linear Velocities - 3R Robot - Example

• DH Parameters



i	α_{i-1}	a_{i-1}	d_i	$ heta_i$
1	0	0	0	θ_1
2	90	L1	0	θ_2
3	0	L2	0	θ_{3}
4	0	L3	0	0





• From the DH parameter table, we can specify the homogeneous transform matrix for each adjacent link pair:

$${}^{i-1}_{i}T = \begin{bmatrix} c\theta_{i} & -s\theta_{i} & 0 & a_{i-1} \\ s\theta_{i}c\alpha_{i-1} & c\theta_{i}c\alpha_{i-1} & -s\alpha_{i-1} & -s\alpha_{i-1}d_{i} \\ s\theta_{i}s\alpha_{i-1} & c\theta_{i}s\alpha_{i-1} & c\alpha_{i-1} & c\alpha_{i-1}d \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^{0}_{1}T = \begin{bmatrix} c1 & -s1 & 0 & 0\\ s1 & c1 & 0 & 0\\ 0 & 0 & 1 & 0\\ 0 & 0 & 0 & 1 \end{bmatrix}$$
$${}^{1}_{2}T = \begin{bmatrix} c2 & -s2 & 0 & L1\\ 0 & 0 & -1 & 0\\ s2 & c2 & 0 & 0\\ 0 & 0 & 0 & 1 \end{bmatrix}$$
$${}^{2}_{3}T = \begin{bmatrix} c3 & -s3 & 0 & L2\\ s3 & c3 & 0 & 0\\ 0 & 0 & 1 & 0\\ 0 & 0 & 0 & 1 \end{bmatrix}$$
$${}^{3}_{4}T = \begin{bmatrix} 1 & 0 & 0 & L3\\ 0 & 1 & 0 & 0\\ 0 & 0 & 1 & 0\\ 0 & 0 & 0 & 1 \end{bmatrix}$$



• The homogeneous transform matrix from frame 0 to each one of the joints (1,2,3,4)

$${}_{1}^{0}T = \begin{bmatrix} c1 & -s1 & 0 & 0 \\ s1 & c1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$
$${}_{2}^{0}T = {}_{1}^{0}T_{2}^{1}T = \begin{bmatrix} c1 & -s1 & 0 & 0 \\ s1 & c1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} c2 & -s2 & 0 & L1 \\ 0 & 0 & -1 & 0 \\ s2 & c2 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} c1c2 & -c1s1 & s1 & L1c1 \\ s1c2 & -s1s2 & -c1 & L1s1 \\ s2 & c2 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$
$${}_{2}^{0}T = {}_{1}^{0}T_{2}^{1}T_{3}^{2}T = \begin{bmatrix} c1 & -s1 & 0 & 0 \\ s1 & c1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} c2 & -s2 & 0 & L1 \\ s2 & c2 & 0 & 0 \\ s2 & c2 & 0 & 0 \\ s2 & c2 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} c3 & -s3 & 0 & L2 \\ s3 & c3 & 0 & 0 \\ s3 & c2 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} c1c23 & -c1s23 & s1 & c1(L1 + L2c2) \\ s1c23 & -s1s23 & -c1 & s1(L1 + L2c2) \\ s23 & c23 & 0 & L2s2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$
$${}_{2}^{0}T = {}_{1}^{0}T_{2}^{1}T_{3}^{2}T_{4}^{3}T = \begin{bmatrix} c1 & -s1 & 0 & 0 \\ s1 & c1 & 0 & 0 \\ s1 & c1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} c2 & -s2 & 0 & L1 \\ s3 & c3 & 0 & 0 \\ s2 & c2 & 0 & 0 \\ s1 & c1 & 0 & 0 \\ s2 & c2 & 0 & 0 \\ s1 & c1 & 0 & 0 \\ s2 & c2 & 0 & 0 \\ s1 & c1 & 0 & 0 \\ s1 & c1 & 0 & 0 \\ s1 & c1 & 0 & 0 \\ s2 & c2 & 0 & 0 \\ s1 & c1 & 0 & 0 \\ s1 & c2 & c2 & 0 & 0 \\ s1 & c1 & 0 & 0 \\ s1 & c1 & 0 & 0 \\ s1 & c1 & 0 & 0 \\ s1 & c2 & c2 & 0 & 0 \\ s1 & c2 & c2 & 0 & 0 \\ s1 & c2 & c2 & 0 & 0 \\ s1 & c2 & c2 & 0 & 0 \\ s1 & c1 & c1 & c1 \\ s1 & c1 & c1 & c1 \\ s1 & c1 & c1 & c1 \\ s2 & c2 & c2 & c1 & s1 \\ s1 & c1 & c1 & c1 \\ s2 & c2 & c2 & c1 & c1 \\ s1 & c1 & c1 & c1 \\ s1 & c$$



• Compute the angular velocity of the end effector frame relative to the base frame expressed at the end effector frame.

$${}^{i+1}\omega_{i+1} = {}^{i+1}_{i}R^{i}\omega_{i} + \begin{bmatrix} 0\\0\\\dot{\theta}_{i+1} \end{bmatrix}$$

$${}^{1}\omega_{1} = {}^{1}_{0}R^{0}\omega_{0} + \begin{bmatrix} 0\\0\\\dot{\theta}_{1} \end{bmatrix} = \begin{bmatrix} c1 & s1 & 0\\-s1 & c1 & 0\\0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0\\0\\0\\0 \end{bmatrix} + \begin{bmatrix} 0\\0\\\dot{\theta}_{1} \end{bmatrix} = \begin{bmatrix} 0\\0\\\dot{\theta}_{1} \end{bmatrix}$$





• For
$$i=1$$

• For $i=1$
• For $i=2$
• For $i=3$
• For $i=1$
• For $i=3$
• Fo

• Note ${}^3\omega_3 = {}^4\omega_4$



- Compute the linear velocity of the end effector frame relative to the base frame expressed at the end effector frame.
- Note that the term involving the prismatic joint has been dropped from the equation (it is equal to zero).

$${}^{i+1}v_{i+1} = {}^{i+1}_{i}R({}^{i}\omega \times {}^{i}P_{i+1} + {}^{i}v_i) + \begin{bmatrix} 0\\ 0\\ d_{i+1} \end{bmatrix}$$



• For *i=0*

$${}^{1}v_{1} = {}^{1}_{0}R\{{}^{0}\omega_{0} \times {}^{0}P_{1} + {}^{0}v_{0}\} = \begin{bmatrix} c1 & s1 & 0\\ -s1 & c1 & 0\\ 0 & 0 & 1 \end{bmatrix} \left\{ \begin{bmatrix} 0\\0\\0\\0 \end{bmatrix} \times \begin{bmatrix} 0\\0\\0\\0 \end{bmatrix} + \begin{bmatrix} 0\\0\\0\\0 \end{bmatrix} \right\} = \begin{bmatrix} 0\\0\\0\\0 \end{bmatrix}$$

• For *i=1*

$${}^{2}v_{2} = {}^{2}_{1}R\{{}^{1}\omega_{1} \times {}^{1}P_{2} + {}^{1}v_{1}\} = \begin{bmatrix} c2 & 0 & s2 \\ -s2 & 0 & c2 \\ 0 & -1 & 0 \end{bmatrix} \left\{ \begin{bmatrix} 0 \\ 0 \\ \dot{\theta}_{1} \end{bmatrix} \times \begin{bmatrix} L1 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \right\} = \begin{bmatrix} 0 \\ 0 \\ -L_{1}\dot{\theta}_{1} \end{bmatrix}$$

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• For *i=3*

$${}^{3}v_{3} = {}^{3}_{2}R\{{}^{2}\omega_{2} \times {}^{2}P_{3} + {}^{2}v_{2}\} = \begin{bmatrix} c3 & s3 & 0 \\ -s3 & c30 & 0 \\ 0 & 0 & 1 \end{bmatrix} \left\{ \begin{bmatrix} s2\dot{\theta}_{1} \\ c2\dot{\theta}_{1} \\ \dot{\theta}_{2} \end{bmatrix} \times \begin{bmatrix} L2 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ -L1\dot{\theta}_{1} \end{bmatrix} \right\}$$
$$= \begin{bmatrix} c3 & s3 & 0 \\ -s3 & c3 & 0 \\ 0 & 0 & 1 \end{bmatrix} \left\{ \begin{bmatrix} 0 \\ L2\dot{\theta}_{1} \\ -L2c2\dot{\theta}_{1} - L1\dot{\theta}_{1} \end{bmatrix} \right\} = \begin{bmatrix} L2s3\dot{\theta}_{2} \\ L2c3\dot{\theta}_{2} \\ (-L1 - L2c2)\dot{\theta}_{1} \end{bmatrix}$$



• For *i=4*

$${}^{4}v_{4} = {}^{4}_{3}R\{{}^{3}\omega_{3} \times {}^{3}P_{4} + {}^{3}v_{3}\}$$

$$= \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \left\{ \begin{bmatrix} s23\dot{\theta}_{1} \\ c23\dot{\theta}_{1} \\ \dot{\theta}_{2} + \dot{\theta}_{3} \end{bmatrix} \times \begin{bmatrix} L3 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} L2s3\dot{\theta}_{2} \\ (-L1 - L2c2)\dot{\theta}_{1} \end{bmatrix} \right\}$$

$$= \begin{bmatrix} L2s3\dot{\theta}_{2} \\ (L2c3 + L3)\dot{\theta}_{2} + L3\dot{\theta}_{3} \\ (-L1 - L2c2 - L3c23)\dot{\theta}_{1} \end{bmatrix}$$



- Note that the linear and angular velocities $({}^4\omega_4, {}^4v_4)$ of the end effector where differentiate (measured) in frame {0} however represented (expressed) in frame {4}
- In the car example: Observer sitting in the "Car" ${}^{C} \begin{bmatrix} {}^{W}V_{C} \end{bmatrix}$ Observer sitting in the "World" ${}^{W} \begin{bmatrix} {}^{W}V_{C} \end{bmatrix}$

$${}^{k}v_{i} \equiv {}^{k} \begin{bmatrix} {}^{0}V_{i} \end{bmatrix} = {}^{k}_{0}R \begin{bmatrix} {}^{0}V_{i} \end{bmatrix} = {}^{k}_{0}R \cdot v_{i}$$
$${}^{k}\omega_{i} \equiv {}^{k} \begin{bmatrix} {}^{0}\Omega_{i} \end{bmatrix} = {}^{k}_{0}R \begin{bmatrix} {}^{0}\Omega_{i} \end{bmatrix} = {}^{k}_{0}R \cdot \omega_{i}$$

Solve for v_4 and ω_4 by multiply both side of the questions from the left by ${}^{4}_{0}R^{-1}$

$${}^{4}\nu_{4} = {}^{4}_{0}R \cdot \nu_{4}$$
$${}^{4}\omega_{4} = {}^{4}_{0}R \cdot \omega_{4}$$





• Multiply both sides of the equation by the inverse transformation matrix, we finally get the linear and angular velocities expressed and measured in the stationary frame {0}

$$v_{4} = {}^{4}_{0}R^{-1} \cdot {}^{4}v_{4} = {}^{4}_{0}R^{T} \cdot {}^{4}v_{4} = {}^{0}_{4}R \cdot {}^{4}v_{4}$$
$$\omega_{4} = {}^{4}_{0}R^{-1} \cdot {}^{4}\omega_{4} = {}^{4}_{0}R^{T} \cdot {}^{4}\omega_{4} = {}^{0}_{4}R \cdot {}^{4}\omega_{4}$$
$${}^{0}_{4}T = {}^{0}_{1}T^{1}_{2}T^{2}_{3}T^{3}_{4}T$$





3R – Example

Analytical Approach – Graphical Interpretation





