

Velocity Propagation Between Robot Links 3/4









Jacobian Matrix - Introduction

• In the field of robotics the Jacobian matrix describe the relationship between the joint angle rates $(\underline{\dot{\theta}}_N)$ and the translation and rotation velocities of the end effector $(\underline{\dot{x}})$. This relationship is given by:

$$\underline{\dot{x}} = J(\underline{\theta})\underline{\dot{\theta}}$$

In addition to the velocity relationship, we are also interested in developing a relationship between the robot joint torques (<u>τ</u>) and the forces and moments (<u>F</u>) at the robot end effector (Static Conditions). This relationship is given by:

$$\underline{\tau} = J(\underline{\theta})^T \underline{F}$$





Jacobian Matrix - Calculation Methods





Summary – Changing Frame of Representation

- Linear and Rotational Velocity - Vector Form ${}^{A}V_{Q} = {}^{A}V_{BORG} + {}^{A}_{B}R^{B}V_{Q} + {}^{A}\Omega_{B} \times {}^{A}_{B}R^{B}P_{Q}$ - Matrix Form ${}^{A}V_{Q} = {}^{A}V_{BORG} + {}^{A}_{B}R^{B}V_{Q} + {}^{A}_{B}\dot{R}_{\Omega} \left({}^{A}_{B}R^{B}P_{Q} \right)$
- Angular Velocity
 - Vector Form

$${}^{A}\Omega_{C} = {}^{A}\Omega_{B} + {}^{A}_{B}R^{B}\Omega_{C}$$

$${}^{A}_{C}\dot{R}_{\Omega} = {}^{A}_{B}\dot{R}_{\Omega} + {}^{A}_{B}R^{B}_{C}\dot{R}_{\Omega}^{A}_{B}R^{T}$$



- As with any vector, a velocity vector may be described in terms of any frame, and this frame of reference is noted with a leading superscript.
- A velocity vector <u>computed</u> in frame {B} and <u>represented</u> in frame {A} would be written







- The homogeneous transform matrix provides a complete description of the linear and angular position relationship between adjacent links.
- These descriptions may be combined together to describe the position of a link relative to the robot base frame {0}.

$${}^{o}_{i}T = {}^{o}_{1}T {}^{1}_{2}T \cdots {}^{i-1}_{i}T$$

• A similar description of the linear and angular velocities between adjacent links as well as the base frame would also be useful.





Position Propagation

${}^{0}_{T}T = {}^{0}_{1}T {}^{1}_{2}T {}^{2}_{3}T {}^{3}_{4}T {}^{4}_{5}T {}^{5}_{6}T {}^{6}_{T}T$

UCLA

Instructor: Jacob Rosen Advanced Robotic - MAE 263D - Department of Mechanical & Aerospace Engineering - UCLA



- In considering the motion of a robot link we will always use link frame {0} as the reference frame (Computed AND Represented). However any frame can be used as the reference (represented) frame including the link's own frame (*i*)
 - Where: v_i is the linear velocity of the origin of link frame (*i*) with respect to frame {0} (Computed AND Represented)
 - ω_i is the angular velocity of the origin of link frame (*i*) with respect to frame {0} (Computed AND Represented)
- Expressing the velocity of a frame {*i*} (associated with link *i*) relative to the robot base (frame {0}) using our previous notation is defined as follows:

$$v_{i} \equiv {}^{0} \left[{}^{0}V_{i} \right] = \left[{}^{0}V_{i} \right]$$
$$\omega_{i} \equiv {}^{0} \left[{}^{0}\Omega_{i} \right] = \left[{}^{0}\Omega_{i} \right]$$



• The velocities differentiate (computed) relative to the base frame $\{0\}$ are often represented relative to other frames $\{k\}$. The following notation is used for this conditions

$${}^{k}v_{i} \equiv {}^{k} \begin{bmatrix} {}^{0}V_{i} \end{bmatrix} = {}^{k}_{0}R \begin{bmatrix} {}^{0}V_{i} \end{bmatrix} = {}^{k}_{0}R \cdot v_{i}$$
$${}^{k}\omega_{i} \equiv {}^{k} \begin{bmatrix} {}^{0}\Omega_{i} \end{bmatrix} = {}^{k}_{0}R \begin{bmatrix} {}^{0}\Omega_{i} \end{bmatrix} = {}^{k}_{0}R \cdot \omega_{i}$$







Velocity Propagation

- Given: A manipulator A chain of rigid bodies each one capable of moving relative to its neighbor
- Problem: Calculate the linear and angular velocities of the link of a robot
- Solution (Concept): Due to the robot structure (serial mechanism) we can compute the velocities of each link in order starting from the base.

The velocity of link i+1 will be that of link i, plus whatever new velocity components were added by joint i+1







• From the relationship developed previously

$${}^{A}\Omega_{C} = {}^{A}\Omega_{B} + {}^{A}_{B}R^{B}\Omega_{C}$$

• we can re-assign link names to calculate the velocity of any link *i* relative to the base frame {0}

$$\begin{cases} A \to 0 \\ B \to i \\ C \to i+1 \end{cases}$$

$${}^{0}\Omega_{i+1} = {}^{0}\Omega_{i} + {}^{0}_{i}R^{i}\Omega_{i+1}$$

• By pre-multiplying both sides of the equation by ${}^{i+1}_{0}R$, we can convert the frame of reference for the base {0} to frame {*i*+1}



$${}^{i+1}_{0}R^{0}\Omega_{i+1} = {}^{i+1}_{0}R^{0}\Omega_{i} + {}^{i+1}_{0}R^{0}_{i}R^{i}\Omega_{i+1}$$

• Using the recently defined notation, we have

$$\omega_{i+1} = \omega_i + \frac{\omega_i + 1}{i} R^i \Omega_{i+1}$$

$${}^{i+1}\omega_{i+1} = \text{Angular velocity of frame } \{i+1\} \text{ measured relative to the robot base, and} \\ = \exp (i+1) + \exp$$



$$^{i+1}\omega_{i+1} = \overset{i+1}{\overset{i+1}{\overset{}}}\omega_i + \overset{i+1}{\overset{i}{\overset{}}}R^i\Omega_{i+1}$$

Angular velocity of frame {i} measured relative to the robot base, expressed in frame {i+1}

 $^{i+1}\omega_i = {}^{i+1}_{i}R^i\omega_i$

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$${}^{i+1}\omega_{i+1} = {}^{i+1}\omega_i + {}^{i+1}R^i\Omega_{i+1}$$

- Angular velocity of frame {*i*+1} measured (differentiate) in frame {*i*} and represented (expressed) in frame {*i*+1}
- Assuming that a joint has only 1 DOF. The joint configuration can be either revolute joint (*angular velocity*) or prismatic joint (Linear velocity).
- Based on the frame attachment convention in which we assign the Z axis pointing along the *i*+1 joint axis such that the two are coincide (rotations of a link is preformed only along its Z- axis) we can rewrite this term as follows:





 The result is a <u>recursive equation</u> that shows the angular velocity of one link in terms of the angular velocity of the previous link plus the relative motion of the two links.

$${}^{i+1}\omega_{i+1} = {}^{i+1}_{i}R^{i}\omega_{i} + \begin{bmatrix} 0\\0\\\dot{\theta}_{i+1}\end{bmatrix}$$

• Since the term ${}^{i+1}\omega_{i+1}$ depends on all previous links through this recursion, the angular velocity is said to propagate from the base to subsequent links.







- Simultaneous Linear and Rotational Velocity
- The derivative of a vector in a moving frame (linear and rotation velocities) as seen from a stationary frame





• From the relationship developed previously (matrix form)

$${}^{A}V_{Q} = {}^{A}V_{BORG} + {}^{A}_{B}R^{B}V_{Q} + {}^{A}_{B}\dot{R}_{\Omega}\left({}^{A}_{B}R^{B}P_{Q}\right)$$

• we re-assign link frames for adjacent links (i and i +1) with the velocity computed relative to the robot base frame {0}

$$\begin{cases} A \to 0 \\ B \to i \\ C \to i + i \end{cases}$$

$${}^{0}V_{i+1} = {}^{0}_{i}\dot{R}_{\Omega} \left({}^{0}_{i}R^{i}P_{i+1} \right) + {}^{0}V_{i} + {}^{0}_{i}R^{i}V_{i+1}$$

• By pre-multiplying both sides of the equation by ${}^{i+1}_{0}R$, we can convert the frame of reference for the left side to frame $\{i+1\}$



$${}^{i+1}_{0}R^{0}V_{i+1} = {}^{i+1}_{0}R^{0}_{i}\dot{R}_{\Omega}^{0} \left({}^{0}_{i}R^{i}P_{i+1}\right) + {}^{i+1}_{0}R^{0}V_{i} + {}^{i+1}_{0}R^{0}_{i}R^{i}V_{i+1}$$

• Which simplifies to

$${}^{i+1}_{0}R^{0}V_{i+1} = {}^{i+1}_{0}R^{0}_{i}\dot{R}_{\Omega} ({}^{0}_{i}R^{i}P_{i+1}) + {}^{i+1}_{0}R^{0}V_{i} + {}^{i+1}_{i}R^{i}V_{i+1}$$

• Factoring out ${}^{i+1}_{i}R$ from the left side of the first two terms

$${}^{i+1}_{0}R^{0}V_{i+1} = {}^{i+1}_{i}R\left({}^{i}_{0}R^{0}_{i}\dot{R}^{0}_{\Omega i}R^{i}P_{i+1} + {}^{i}_{0}R^{0}V_{i}\right) + {}^{i+1}_{i}R^{i}V_{i+1}$$

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$${}^{i+1}_{0}R^{0}V_{i+1} = {}^{i+1}_{i}R\left({}^{i}_{0}R^{0}_{i}\dot{R}^{0}_{\Omega i}R^{i}P_{i+1} + {}^{i}_{0}R^{0}V_{i}\right) + {}^{i+1}_{i}R^{i}V_{i+1}$$

 ${}^{i+1}_{i}R^{i}V_{i+1}$ - Linear velocity of frame $\{i+1\}$ measured relative to frame $\{i\}$ and expressed in frame $\{i+1\}$

- Assuming that a joint has only 1 DOF. The joint configuration can be either revolute joint (angular velocity) or prismatic joint (Linear velocity).
- Based on the frame attachment convention in which we assign the Z axis pointing along the *i*+1 joint axis such that the two are coincide (translation of a link is preformed only along its Z- axis) we can rewrite this term as follows:

$${}^{i+1}_{i}R^{i}V_{i+1} = \begin{bmatrix} 0\\0\\\dot{d}_{i+1} \end{bmatrix}$$



Velocity of Adjacent Links - Linear Velocity 5/6

$$\overset{i+1}{}_{0}R^{0}V_{i+1} = \overset{i+1}{}_{i}R (\overset{i}{}_{0}R^{0}\dot{R}_{\Omega i}R^{0}R^{i}P_{i+1} + \overset{i}{}_{0}R^{0}V_{i}) + \begin{bmatrix} 0\\0\\\dot{d}_{i+1}\end{bmatrix}$$







 The result is a <u>recursive equation</u> that shows the linear velocity of one link in terms of the previous link plus the relative motion of the two links.

$${}^{i+1}v_{i+1} = {}^{i+1}_{i}R({}^{i}\omega_{i}\times{}^{i}P_{i+1} + {}^{i}v_{i}) + \begin{bmatrix} 0\\0\\\dot{d}_{i+1} \end{bmatrix}$$

• Since the term ${}^{i+1}V_{i+1}$ depends on all previous links through this recursion, the angular velocity is said to propagate from the base to subsequent links.



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Velocity of Adjacent Links - Summary

• Angular Velocity





Angular and Linear Velocities - 3R Robot - Example

• For the manipulator shown in the figure, compute the angular and linear velocity of the "tool" frame relative to the base frame expressed in the "tool" frame (that is, calculate ${}^4\omega_4$ and 4v_4).







• Frame attachment







• DH Parameters



i	α_{i-1}	a_{i-1}	d_i	$ heta_i$
1	0	0	0	θ_1
2	90	L1	0	θ_2
3	0	L2	0	θ_3
4	0	L3	0	0



• From the DH parameter table, we can specify the homogeneous transform matrix for each adjacent link pair:

$${}^{i-1}_{i}T = \begin{bmatrix} c\theta_{i} & -s\theta_{i} & 0 & a_{i-1} \\ s\theta_{i}c\alpha_{i-1} & c\theta_{i}c\alpha_{i-1} & -s\alpha_{i-1} & -s\alpha_{i-1}d_{i} \\ s\theta_{i}s\alpha_{i-1} & c\theta_{i}s\alpha_{i-1} & c\alpha_{i-1} & c\alpha_{i-1}d \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^{0}_{1}T = \begin{bmatrix} c1 & -s1 & 0 & 0 \\ s1 & c1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} {}^{1}_{2}T = \begin{bmatrix} c2 & -s2 & 0 & L1 \\ 0 & 0 & -1 & 0 \\ s2 & c2 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^{2}_{3}T = \begin{bmatrix} c3 & -s3 & 0 & L2 \\ s3 & c3 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} {}^{3}_{4}T = \begin{bmatrix} 1 & 0 & 0 & L3 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

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• Compute the angular velocity of the end effector frame relative to the base frame expressed at the end effector frame.

$${}^{i+1}\omega_{i+1} = {}^{i+1}_{i}R^{i}\omega_{i} + \begin{bmatrix} 0\\0\\\dot{\theta}_{i+1} \end{bmatrix}$$

• For *i=0*

$${}^{1}\omega_{1} = {}^{1}_{0}R^{0}\omega_{0} + \begin{bmatrix} 0\\0\\\dot{\theta}_{1} \end{bmatrix} = \begin{bmatrix} c1 & s1 & 0\\-s1 & c1 & 0\\0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0\\0\\0\\\dot{\theta}_{1} \end{bmatrix} + \begin{bmatrix} 0\\0\\\dot{\theta}_{1} \end{bmatrix} = \begin{bmatrix} 0\\0\\\dot{\theta}_{1} \end{bmatrix}$$

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• For
$$i=1$$

 ${}^{2}\omega_{2}={}^{2}_{1}R^{1}\omega_{1}+\begin{bmatrix}0\\0\\\dot{\theta}_{2}\end{bmatrix}=\begin{bmatrix}c2&0&s2\\-s2&0&c2\\0&-1&0\end{bmatrix}\begin{bmatrix}0\\0\\\dot{\theta}_{1}\end{bmatrix}+\begin{bmatrix}0\\0\\\dot{\theta}_{2}\end{bmatrix}=\begin{bmatrix}s2\dot{\theta}_{1}\\c2\dot{\theta}_{1}\\\dot{\theta}_{2}\end{bmatrix}$
• For $i=2$
 ${}^{3}\omega_{3}={}^{3}_{2}R^{2}\omega_{2}+\begin{bmatrix}0\\0\\\dot{\theta}_{3}\end{bmatrix}=\begin{bmatrix}c3&s3&0\\-s3&c3&0\\0&0&1\end{bmatrix}\begin{bmatrix}s2\dot{\theta}_{1}\\c2\dot{\theta}_{1}\\\dot{\theta}_{2}\end{bmatrix}+\begin{bmatrix}0\\0\\\dot{\theta}_{3}\end{bmatrix}=\begin{bmatrix}s23\dot{\theta}_{1}\\c23\dot{\theta}_{1}\\\dot{\theta}_{2}+\dot{\theta}_{3}\end{bmatrix}$
• For $i=3$
 ${}^{4}\omega_{4}={}^{4}_{3}R^{3}\omega_{3}+\begin{bmatrix}0\\0\\0\end{bmatrix}=\begin{bmatrix}1&0&0\\0&1&0\\0&0&1\end{bmatrix}\begin{bmatrix}s23\dot{\theta}_{1}\\c23\dot{\theta}_{1}\\\dot{\theta}_{2}+\dot{\theta}_{3}\end{bmatrix}+\begin{bmatrix}0\\0\\0\end{bmatrix}=\begin{bmatrix}s23\dot{\theta}_{1}\\c23\dot{\theta}_{1}\\\dot{\theta}_{2}+\dot{\theta}_{3}\end{bmatrix}$

• Note ${}^{3}\omega_{3} = {}^{4}\omega_{4}$



Angular and Linear Velocities - 3R Robot - Example

- Compute the linear velocity of the end effector frame relative to the base frame expressed at the end effector frame.
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- Note that the term involving the prismatic joint has been dropped from the equation (it is equal to zero).

$${}^{i+1}v_{i+1} = {}^{i+1}_{i}R(i\omega \times {}^{i}P_{i+1} + {}^{i}v_i) + \begin{bmatrix} 0\\0\\\dot{d}_{i+1} \end{bmatrix}$$



• For *i=0*

$${}^{1}v_{1} = {}^{1}_{0}R\left\{{}^{0}\omega_{0}\times{}^{0}P_{1} + {}^{0}v_{0}\right\} = \begin{bmatrix} c1 & s1 & 0\\ -s1 & c1 & 0\\ 0 & 0 & 1 \end{bmatrix} \left\{ \begin{bmatrix} 0\\0\\0\\0 \end{bmatrix} \times \begin{bmatrix} 0\\0\\0\\0 \end{bmatrix} + \begin{bmatrix} 0\\0\\0\\0 \end{bmatrix} \right\} = \begin{bmatrix} 0\\0\\0\\0 \end{bmatrix}$$

• For *i=1*

$${}^{2}v_{2} = {}^{2}_{1}R\left\{{}^{1}\omega_{1}\times{}^{1}P_{2} + {}^{1}v_{1}\right\} = \begin{bmatrix} c2 & 0 & s2 \\ -s2 & 0 & c2 \\ 0 & -1 & 0 \end{bmatrix} \left\{\begin{bmatrix} 0 \\ 0 \\ \dot{\theta}_{1} \end{bmatrix} \times \begin{bmatrix} L1 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}\right\} = \begin{bmatrix} 0 \\ 0 \\ -L_{1}\dot{\theta}_{1} \end{bmatrix}$$



• For *i=3*

$${}^{3}v_{3} = {}^{3}_{2}R\left\{{}^{2}\omega_{2}\times{}^{2}P_{3} + {}^{2}v_{2}\right\} = \begin{bmatrix} c3 & s3 & 0\\ -s3 & c30 & 0\\ 0 & 0 & 1 \end{bmatrix} \left\{ \begin{bmatrix} s2\dot{\theta}_{1}\\ c2\dot{\theta}_{1}\\ \dot{\theta}_{2} \end{bmatrix} \times \begin{bmatrix} L2\\ 0\\ 0 \end{bmatrix} + \begin{bmatrix} 0\\ 0\\ -L1\dot{\theta}_{1} \end{bmatrix} \right\}$$
$$= \begin{bmatrix} c3 & s3 & 0\\ -s3 & c3 & 0\\ 0 & 0 & 1 \end{bmatrix} \left\{ \begin{bmatrix} 0\\ L2\dot{\theta}_{1}\\ -L2c2\dot{\theta}_{1} - L1\dot{\theta}_{1} \end{bmatrix} \right\} = \begin{bmatrix} L2s3\dot{\theta}_{2}\\ L2c3\dot{\theta}_{2}\\ (-L1 - L2c2)\dot{\theta}_{1} \end{bmatrix}$$



• For *i=4*

$${}^{4}v_{4} = {}^{4}_{3}R \left\{ {}^{3}\omega_{3} \times {}^{3}P_{4} + {}^{3}v_{3} \right\} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \left\{ \begin{bmatrix} s23\dot{\theta}_{1} \\ c23\dot{\theta}_{1} \\ \dot{\theta}_{2} + \dot{\theta}_{3} \end{bmatrix} \times \begin{bmatrix} L3 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} L2s3\dot{\theta}_{2} \\ (-L1 - L2c2)\dot{\theta}_{1} \end{bmatrix} \right\}$$
$$= \begin{bmatrix} L2s3\dot{\theta}_{2} \\ (L2c3 + L3)\dot{\theta}_{2} + L3\dot{\theta}_{3} \\ (-L1 - L2c2 - L3c23)\dot{\theta}_{1} \end{bmatrix}$$



Angular and Linear Velocities - 3R Robot - Example

- Note that the linear and angular velocities (${}^4\omega_4, {}^4\nu_4$) of the end effector where differentiate (measured) in frame {0} however represented (expressed) in frame {4}
- In the car example: Observer sitting in the "Car"

Observer sitting in the "World"

$${}^{C} \begin{bmatrix} {}^{W}V_{C} \end{bmatrix}$$
$${}^{W} \begin{bmatrix} {}^{W}V_{C} \end{bmatrix}$$

$${}^{k}v_{i} \equiv {}^{k} \begin{bmatrix} {}^{0}V_{i} \end{bmatrix} = {}^{k}_{0}R \begin{bmatrix} {}^{0}V_{i} \end{bmatrix} = {}^{k}_{0}R \cdot v_{i}$$
$${}^{k}\omega_{i} \equiv {}^{k} \begin{bmatrix} {}^{0}\Omega_{i} \end{bmatrix} = {}^{k}_{0}R \begin{bmatrix} {}^{0}\Omega_{i} \end{bmatrix} = {}^{k}_{0}R \cdot \omega_{i}$$

Solve for v_4 and ω_4 by multiply both side of the questions from the left by ${}^4_0 R^{-1}$

$${}^{4}v_{4} = {}^{4}_{0}R \cdot v_{4}$$
$${}^{4}\omega_{4} = {}^{4}_{0}R \cdot \omega_{4}$$



 Multiply both sides of the equation by the inverse transformation matrix, we finally get the linear and angular velocities expressed and measured in the stationary frame {0}

$$v_{4} = {}_{0}^{4}R^{-1} \cdot {}^{4}v_{4} = {}_{0}^{4}R^{T} \cdot {}^{4}v_{4} = {}_{4}^{0}R \cdot {}^{4}v_{4}$$
$$\omega_{4} = {}_{0}^{4}R^{-1} \cdot {}^{4}\omega_{4} = {}_{0}^{4}R^{T} \cdot {}^{4}\omega_{4} = {}_{4}^{0}R \cdot {}^{4}\omega_{4}$$
$${}_{4}^{0}T = {}_{1}^{0}T {}_{2}^{1}T {}_{3}^{2}T {}_{4}^{3}T$$































Angular and Linear Velocities - 3R Robot - Example





Angular and Linear Velocities - 3R Robot - Example



